



Application for Conditional Use Permit

Applicant Name:	
Address:	City:
State: Zip:	
Telephone:	Cell Phone:
Email:	
Agent Name:	
Address:	City:
State: Zip:	
Telephone:	Cell Phone:
Email:	
Property Address (Es):	
Current Zoning:	
Current/Most Recent Property Use:	
Proposed Use:	









The application will be evaluated using the standards of Sec. 114-154 of the Municipal Code (below). Please use the space to justify and explain how your proposal addresses these conditions; use an additional sheet if necessary.

- (1) The establishment, maintenance, or operation of the conditional use will not be detrimental to, or endanger, the public health, safety, morals, comfort, or general welfare:
- (2) The conditional use will not be injurious to the use and enjoyment of other property in the immediate vicinity for the purposes already permitted, nor substantially diminish and impair property values within the neighborhood;
- (3) The establishment of the conditional use will not impede the normal and orderly development and improvement of the surrounding property for uses permitted in the district:
- (4) Adequate utilities, access roads, drainage and/or necessary facilities have been or are being provided;
- (5) Adequate measures have been or will be taken to provide ingress and egress so designed as to minimize traffic congestion in the public streets;
- (6) The proposed conditional use is not contrary to the objectives of the current land use plan for the city; and
- (7) The conditional use shall, in all other respects, conform to the applicable regulations of the district in which it is located, except as such regulations may, in each instance, be modified pursuant to the recommendations of the plan commission.









If the required supplemental materials, which constitute a completed application, are not submitted, the application will not be processed.

Required Submittal Format

1. An electronic submission via email/USB drive/CD/Download link; and

2. One (1) paper copy, no larger than 11" x 17" size.

Required Submittal Item	Applicant	City
	Submitted	Received
1. Conditional Use Review Application		
2. Written description of project, including:		
a. Hours of operation		
b. Anticipated delivery schedule		
c. Maintenance plan		
d. General use of the building and lot		
3. Site Plan (drawn to scale), including:		
a. Fully dimensioned property boundary		
b. All buildings (existing and proposed)		
c. Setbacks from property lines		
d. Identification as to whether all elements are "Existing" or		
"Proposed"		
e. Dimensioned parking spaces and drive aisle layout		
f. Trash enclosure location and materials		
g. Loading spaces		
h. Fire hydrant locations		
i. Location of signage, with setbacks		
4. Zoning Analysis Table		
a. Land area (in acres and square feet)		
b. Building area (in square feet)		
c. Setbacks (required yards in feet)		
d. Floor Area Ratio (building area divided by lot area)		
e. Lot Coverage (building footprint divided by lot area)		
f. Height of all buildings and structures		
g. Percentage of greenspace (landscaped areas divided by lot area)		
h. Parking spaces		
5. Landscape Plan		
a. Bufferyards		
b. Parking Areas		
c. Screening and fencing locations		
d. Plant lists including the following: Latin and Common Names,		
Number of each planting material, and Size at planting.		







DFPARTMENT OF

CITY NEVELOPMENT



Required Submittal Item	Applicant Submitted	City Received
6. Lighting Plan		
b. A cut sheet of light fixtures with indication of cut-offs or shielding		
c. Illumination diagram indicating intensity of lighting on the		
property.		
7. Floor Plan		
a. Preliminary floor plan layout of all buildings/structures		
b. Labels for the type of use of the area		
c. Labels for square footage of the area		
8. Engineering Plan		
a. Stormwater Plan (Drainage pattern, flow, detention)		
b. Existing and proposed roadway and access configurations		
c. Cross access		
9. Signage Plan		
a. dimensioned color elevations of signage		
b. A diagram showing the location of the proposed signage		
10. Building/site elevations (if new building or exterior changes planned)		
a. Building elevations showing all four sides of the buildings in		
color		
b. Elevation of trash enclosure area		
11. Building Material Samples (if making exterior changes)	 ✓ 	
12. Review Fee	~	

Acknowledgement and authorization signatures

A conditional use is not like a building permit; applying does not mean it will be approved.

The approval may contain conditions related to the improvement of the site which must be met prior to the issuance of a building occupancy permit. Conditions related to the operational aspect(s) of the business must be complied with at all times. That, in the event site improvement work required by ordinance cannot be completed prior to desired occupancy, a financial assurance, at 100% of the improvement estimate, guaranteeing completion of the required improvements must be placed on file with the City of Racine. Estimates and Assurance documents are subject to the review and final approval by the City. Improvements may include but are not limited to landscaping, fencing, lighting, pavement surfacing and sealing, dumpster enclosures, and exterior building improvements;

The signature(s) hereby certify that the statements made by myself and constituting part of this application are true and correct. I am fully aware that any misrepresentation of any information on this application may be grounds for denial of this application.

Owner Signature (acknowledgement and authorization):

Applicant Signature (acknowledgement):

Date: 8(0/22

July 18, 2022 Date:



Joe Goldshlack







<u>NOTES</u>	
 CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS. CONTRACTOR SHALL MAINTAIN A 10'-0" MINIMUM SEPARATION BETWEEN THE PROPOSED GPS UNIT, TRANSMITTING ANTENNAS AND EXISTING GPS UNITS. 	dish
	5701 SOUTH SANTA FE DRIVE LITTLETON, CO 80120
	FULLERTON NIOU E. WOODFIELD ROAD, SUITE 500 SCHAUMBURG, ILLINOIS 60173 TEL: 847-908-8400 COA# 3620-11 www.FullertonEngineering.com
	DANIEL W. SMITH 44096-6 SCHAUMBURG, W
	IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECTION OF A LICENSED PROFESSIONAL ENGINEER, TO ALTER THIS DOCUMENT. DRAWN BY: CHECKED BY: APPROVED BY: LA DZ DS
	RFDS REV #: 2 PERMITTING DOCUMENTS
	SUBMITTALS REV DATE DESCRIPTION A 03/31/2022 Issued for review B 05/11/2022 Issued for review 0 07/07/2022 Issued for review 0 07/07/2022 Issued for review
	A&E PROJECT NUMBER 2021.0030.0004 DISH Wireless L.L.C. PROJECT INFORMATION
	MWMKE00116B 314 6TH STREET RACINE, WI 53403 SHEET TITLE
	OVERALL SITE PLAN SHEET NUMBER
12' 8' 4' 0 10' 20' 3/32"=1'-0"	A-1



ENLARGED BUILDING PLAN

<u>NOTES</u>

1. CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS.

2. CONTRACTOR SHALL MAINTAIN A 10'-0" MINIMUM SEPARATION BETWEEN THE PROPOSED GPS UNIT, TRANSMITTING ANTENNAS AND EXISTING GPS UNITS.

3. CONTRACTOR TO VERIFY WITH DISH Wireless L.L.C. C.M. THE LOCATION OF THE POWER AND FIBER SOURCE PRIOR TO CONSTRICTION.

4. UTILITY RUBBER MAT TO BE IN STALLED UNDER ALL DISH Wireless L.L.C. EQUIPMENT THAT IS RESTING ON OR AFFIXED TO ROOF MEMBRANE



6' 4' 2' 0 5' 10' 3/16"=1'-0"





ENLARGED EQUIPMENT PLAN



12"6"0

2' 3'

1/2"=1'-0'





	<u>NOTES</u>	
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		5701 SOUTH SANTA FE DRIVE LITTLETON, CO 80120
		ULLERTON
CHAUMBURG, LLING 60/73 CAR BOOL DISH WRELESS ANTENNAS RAD CENTER © 59-0'-2 AGL CAR BOOL CONTRACT WALL CONTRACT WALL) PROPOSED DISH WIRELESS ANTENNAS TOP • 62'-0"± AGL	1100 E. WOODFIELD ROAD, SUITE 500
EXISTING PARAPET WALL TOP @ 55-0'± AGL) PROPOSED DISH WRELESS ANTENNAS	SCHAUMBURG, ILLINOIS 60173 TEL: 847-908-8400 COA# 3620-11
	EXISTING PARAPET WALL TOP @ 55'-0"± AGL	www.FullertonEngineering.com
	EXISTING BUILDING ROOF TOP @ 49'-4"± AGL	DANIEL W. SMITH 44096-6 SCHAUMBURG, U
0 07/07/2022 ISSUED FOR PERMITTING 0 07/07/2022 ISSUED FOR PERMITTING 0 07/07/2022 ISSUED FOR PERMITTING 0 A&E PROJECT NUMBER 2021.0030.0004 DISH Wireless LL.C. PROJECT INFORMATION MWMKE00116B 314 6TH STREET RACINE, WI 53403 SHEET TITLE BUILDING ELEVATION SHEET NUMBER A-4 6' 4' 2' 3/16''=1'-0'' 10'	EXISTING BUILDING	IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECTION OF A LICENSED PROFESSIONAL ENGINEER, TO ALTER THIS DOCUMENT. DRAWN BY: CHECKED BY: APPROVED BY: LA DZ DS RFDS REV #: 2 PERMITTING DOCUMENTS SUBMITTALS REV DATE DESCRIPTION A 03/31/2022 ISSUED FOR REVIEW B 05/11/2022 ISSUED FOR REVIEW
6' 4' 2' 0 5' 10' 3/16"=1'-0"	 O'−O"± AGL	B 05/11/2022 ISSUED FOR REVIEW 0 07/07/2022 ISSUED FOR PERMITTING A&E PROJECT NUMBER 2021.0030.0004 DISH Wireless L.L.C. PROJECT INFORMATION MWMKE00116B 314 6TH STREET RACINE, WI 53403 SHEET TITLE BUILDING ELEVATION SHEET NUMBER A
3/16"=1'-0"	6' 4' 2' 0 5' 10'	A-4
	3/16"=1'-0"	













<u>NOTES</u>					
AS PERFORMED ALL REQUIRED SHO RATINGS FOR EACH DEVICE IS AD ICTRICAL SYSTEM.	ORT CIRCUIT EQUATE TO PRO	DTECT			
AS PERFORMED ALL REQUIRED VOL ICH CIRCUIT AND FEEDERS COMPL 0.19(A)(1) FPN NO. 4.	TAGE DROP Y WITH THE NE				
CURRENT CARRYING CONDUCTORS 80% PER 2014/17 NEC TABLE 31 UL1015 WIRE.	EACH, SHALL A 0.15(B)(3)(a) (wireless.			
15A-20A/1P BREAKER: 0.8 x 3 25A-30A/2P BREAKER: 0.8 x 4 35A-40A/2P BREAKER: 0.8 x 5 45A-60A/2P BREAKER: 0.8 x 7	0A = 24.0A 0A = 32.0A 5A = 44.0A 5A = 60.0A		5701 SOUTH SANTA FE DRIVE LITTLETON, CO 80120		
PER NEC CHAPTER 9, TABLE 4, 122 SQ. IN AREA 213 SQ. IN AREA 316 SQ. IN AREA 907 SQ. IN AREA	ARTICLE 358.				
T CONDUCTORS (1 CONDUIT): USI	NG THWN-2, CU).			
0211 SQ. IN X 2 = 0.0422 SQ. IN 0211 SQ. IN X 1 = 0.0211 SQ. IN	I <ground< td=""><td></td><td>I 100 E. WOODFIELD ROAD, SUITE 500 SCHAUMBURG, ILLINOIS 60173</td></ground<>		I 100 E. WOODFIELD ROAD, SUITE 500 SCHAUMBURG, ILLINOIS 60173		
= 0.0633 SQ. II O HANDLE THE TOTAL OF (3) WIR	ES,		TEL: 847-908-8400 COA# 3620-11 www.FullertonEngineering.com		
INDICATED ABOVE.					
0266 SQ. IN X 4 = 0.1064 SO II	N				
0082 SQ. IN X 1 = 0.0082 SQ. II	i ⊲BARE GROUN	ND	MULL.		
= 0.1146 SQ. IN TO HANDLE THE TOTAL OF (5) WI INDICATED ABOVE.	RES,		WISCONS N.		
ONDUIT): USING THWN, CU.			DANIEL W. SMITH		
0.2679 SQ. IN X 3 = 0.8037 SQ. 0.2043 SQ. IN X 1 = 0.2043 SO	IN IN <ground< td=""><td></td><td>44096-6 gr</td></ground<>		44096-6 gr		
= 1.0080 SQ.	N		-D. SCHAUMBURG, W		
O HANDLE THE TOTAL OF (4) WIR INDICATED ABOVE.	ES,		Delet Are Contin		
RVICE CONDUCTOR: D MAY BE USED INSTEAD OF 3/0 CU -	+ #4 GRD IF THE	TOTAL	in the second se		
CONDUCTOR IS LESS THAN 300 FT FRO CTORS MUST BE 90°C TO CARRY THE F	ULL 200A LOAD	NER. REQUIRED			
PPER BUSS CONNECTIONS MUST MEET A D. USE ANTI CORROSION CONDUCTIVE L	AND CONFORM TO UBRICANT ON CON	ANSI INECTIONS	UNLESS THEY ARE ACTING UNDER THE DIRECTION OF A LICENSED PROFESSIONAL ENGINEER, TO ALTER THIS DOCUMENT.		
	NO SCALE		DRAWN BY: CHECKED BY: APPROVED BY:		
	GUNEL		LA DZ DS		
			RFDS REV #: 2		
			PERMITTING		
			DOCUMENTS		
			SUBMITTALS		
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			A&E PROJECT NUMBER		
			2021.0030.0004		
		DISH Wireless L.L.C. PROJECT INFORMATION			
			MWMKF00116B		
			314 6TH STREET RACINE, WI 53403		
			SHEET TITLE		
			ELECTRICAL ONE-LINE AND PANEL SCHEDULE		
			SHEET NUMBER		
			E-3		
	NO SCALE	3			





HYBRID/DISCREET CABLES			3/4" TAPE	WIDTHS WITH 3/	4" SPACING					ORANGE
LOW-BAND RRH (600 MHz N71 BASEBAND) + (850 MHz N26 BAND) + (700 MHz N29 BAND) - OPTIONAL PER MARKET	PORT 1 + SLANT - SLAN	PHA RRH 2 PORT 3 POR IT + SLANT - SL	T 4 ANT + SLANT	BETA RRH PORT 2 - SLANT + SLANT	PORT 4 - SLANT + S	ORT 1 POR SLANT - SI	CAMMA RRH T 2 PORT 3 ANT + SLANT	PORT 4 - SLANT		
ADD FREQUENCY COLOR TO SECTOR BAND (CBRS WILL USE YELLOW BAND)	RED RED ORANGE ORANG	E RED RE	ED BLUE	ORANGE BLUE	BLUE GF		REN GREEN	GREEN		CBRS TECH (3 GHz) YELLOW
										ALPHA SECTOR
MID-BAND RRH (AWS BANDS N66+N70)	RED	RED	BLUE	BLUE	BLUE	REEN	GREEN	GREEN		RED
ADD FREQUENCY COLOR TO SECTOR BAND (CBRS WILL USE YELLOW BANDS)	PURPLE PURPL	E RED RE	PURPLE	PURPLE BLUE	BLUE PU PURPLE		PLE GREEN	GREEN PURPLE	-	COLOR IDENTIFIER
								(-) PORT	F	
HYBRID/DISCREET CABLES INCLUDE SECTOR BANDS BEING SUPPORTED ALONG WITH FREQUENCY BANDS.	EXAMPLE 1	EXAMPLE 2	EXAMPLE 3 COAX#1 (ALPHA)	CANISTER COAX #2 (ALPHA)						
EXAMPLE 1 - HYBRID, OR DISCREET, SUPPORTS ALL SECTORS, BOTH LOW-BANDS AND MID-BANDS.	RED BLUE	RED BLUE	RED	RED						
EXAMPLE 2 - HYBRID, OR DISCREET, SUPPORTS CBRS ONLY, ALL SECTORS.	GREEN	GREEN		RED						
EXAMPLE 3 $-$ main coax with ground mounted RRHs .	ORANGE PURPLE	YELLOW								
FIBER JUMPERS TO RRHS LOW-BAND HHR FIBER CABLES HAVE SECTOR STRIPE ONLY.	LOW BAND RRH	MID BAND RRH	LOW BAND RR	H MID BAND R	RH LOW B	AND RRH	MID BAND RRH	ł		
POWER CABLES TO RRHs		MID BAND RRH				AND RRH		4		
LOW-BAND RRH POWER CABLES HAVE SECTOR STRIPE ONLY	RED	RED	BLUE	BLUE	GF	REEN	GREEN			
	ORANGE	PURPLE	ORANGE	PURPLE		ANGE	PORPLE			<u>NOT USED</u>
RET MOTORS AT ANTENNAS RET CONTROL IS HANDLED BY THE MID-BAND RRH WHEN ONE SET OF RET PORTS EXIST ON	ANTENNA ANTENN 1 1 MID BAND LOW BA	IA ND	ANTENNA 1 MID BAND L	ANTENNA 1 OW BAND	ANT MID	TENNA ANTE 1 BAND LOW	NNA BAND			
SEPARATE RET CABLES ARE USED WHEN ANTENNA PORTS PROVIDE INPUTS FOR BOTH LOW AND MID BANDS.	RED RED PURPLE ORANG	E	BLUE	BLUE	GF	REEN GRI	EN NGE			
MICROWAVE RADIO LINKS	FORWARD AZIMU	TH OF 0-120 DEGRE	ES FORWARD	AZIMUTH OF 120-24	D DEGREES FO	RWARD AZIM	JTH OF 240-359	DEGREES		
LINKS WILL HAVE A 1.5-2 INCH WHITE WRAP WITH THE AZIMUTH COLOR OVERLAPPING IN	PRIMARY SECONDA		PRIMARY S	LCONDARY	PRI	MARY SECON				
THE MIDDLE. ADD ADDITIONAL SECTOR COLOR BANDS FOR EACH ADDITIONAL MW RADIO.	WHITE WHITE		WHITE	WHITE	W	HITE WH	TE			
MICROWAVE CABLES WILL REQUIRE P-TOUCH LABELS INSIDE THE CABINET TO IDENTIFY THE LOCAL AND REMOTE SITE ID'S.	WHITE WHITE		WHITE	WHITE BLUE WHITE	s ▼/ /		TE TE			

[AWS (N66+N70+H-BLOCK) PURPLE NEGATIVE SLANT PORT ON ANT/RRH WHITE		STOL SOUTH SANTA FE DRIVE LITTLETON, CO 80120
TOR	GAMMA SECTOR GREEN	-	VULLERTON NI00 E. WOODFIELD ROAD, SUITE 500 SCHAUMBURG, ILLINOIS 60173 TEL: 847-908-8400 COA# 3620-11 www.FullertonEngineering.com
	NO SCALE	2	DANIEL W. DANIEL W. SMITH 44096-6 SCHAUMBURG, W. IL SCHAUMBURG, W. IL SCHAUMBURG, W. IL SCHAUMBURG, W. IL SCHAUMBURG, W. IL IL SCHAUMBURG, W. SMITH ADDOC NOT LAW FOR ANY PERSON, IL SUBMITTALS
			REV DATE DESCRIPTION A 03/31/2022 ISSUED FOR REVIEW B 05/11/2022 ISSUED FOR REVIEW O 07/07/2022 ISSUED FOR PERMITTING A&E PROJECT NUMBER 2021.0030.0004 DISH Wireless LLC. PROJECT INFORMATION MWMKE00116B 314 6TH STREET RACINE, WI 53403 SHEET TITLE RF CABLE COLOR CODE SHEET NUMBER RF-1
	NO SCALE	4	

EXOTHERMIC CONNECTION	•	AB	ANCHOR BOLI	IN
MECHANICAL CONNECTION		ABV	ABOVE	IN I LB(S)
BUSS BAR INSULATOR	A	ADDL	ADDITIONAL	LB(3)
	- A	AFF	ABOVE FINISHED FLOOR	LTE
	₩ Ω.	AFG	ABOVE FINISHED GRADE	MAS
		AGL	ABOVE GROUND LEVEL	MAX
EXCINERMIC WITH INSPECTION SLEEVE		ALUM	ALUMINUM	MECH
GROUNDING BAR		ALT	ALTERNATE	MFR
GROUND ROD	ı ⊢●	ANT	ANTENNA	MGB
TEST GROUND ROD WITH INSPECTION SLEEVE	୲│──ᡚ⊤	APPROX	APPROXIMATE	MIN
	4	ARCH	AUTOMATIC TRANSFER SWITCH	MISC
SINGLE FOLE SWITCH	Þ	AWG	AMERICAN WIRE GAUGE	MTS
DUPLEX RECEPTACLE	Щ	BATT	BATTERY	MW
	Ψ	BLDG	BUILDING	NEC
DUPLEX GFCI RECEPTACLE	(F)	BLK	BLOCK	NM
FLUORESCENT LIGHTING FIXTURE (2) TWO LAMPS 48		BM	BEAM	NO. #
		BTC	BARE TINNED COPPER CONDUCTOR	" NTS
SMOKE DETECTION (DC)	SD	BOF	BOTTOM OF FOOTING	OC
	\smile	CAB		OSHA
EMERGENCY LIGHTING (DC)		CHG	CHARGING	OPNG
SECURITY LIGHT W/PHOTOCELL LITHONIA AL YW	$\overline{}$	CLG	CEILING	PCS
LED-1-25A400/51K-SR4-120-PE-DDBTXD		CLR	CLEAR	PCU
CHAIN LINK FENCE	x x x x	COL	COLUMN	PRC
WOOD/WROUGHT IRON FENCE	- <u>ooo</u> oo	COMM	CONCRETE	PP
WALL STRUCTURE		CONSTR	CONSTRUCTION	PSF
FASE AREA		DBL	DOUBLE	PT
		DC		PWR
RUPERIT LINE (PL)			DEPARIMENT DOUGLAS FIR	QTY
LIBACKS		DIA	DIAMETER	RAD
JE BRIDGE		DIAG	DIAGONAL	REF
CABLE TRAY		DIM	DIMENSION	REINF
WATER LINE	w w w w w	DWG	DRAWING DOWEL	REQ'D
JNDERGROUND POWER	UGP UGP UGP	EA	EACH	RET
UNDERGROUND TELCO	—— UGT —— UGT —— UGT —— UGT ——	EC	ELECTRICAL CONDUCTOR	RF
VERHEAD POWER		EL.	ELEVATION	RRH
VERHEAD TELCO	OHT OHT OHT	ELEC		RRU
NDERGROUND TELCO/POWER		ENG	ENGINEER	RWY
		EQ	EQUAL	SCH
		EXP	EXPANSION	SIAD
	AGI AGI AGI AGI AGI AGI AGI	EXT		SIM
ABOVE GROUND TELCO/POWER	—— AGT/P — AGT/P — AGT/P — AGT/P ——	EW FAR	LAUH WAY	SPEC
WORKPOINT	W.P.	FF	FINISH FLOOR	SQ
SECTION REFERENCE		FG	FINISH GRADE	SS ATD
	x-x	FIF	FACILITY INTERFACE FRAME	STL
	-	FIN	FINISH(ED)	TEMP
	XX	FLR FDN		ТНК
DETAIL REFERENCE	$\left(\frac{\hat{x}}{x-x}\right)$	FOC	FACE OF CONCRETE	TMA
	\smile	FOM	FACE OF MASONRY	IN TO▲
		FOS	FACE OF STUD	тос
		FOW	FACE OF WALL	TOF
		FS FT	FINISH SURFACE	TOP
		FTG	FOOTING	TOS
		GA	GAUGE	TOW
		GEN	GENERATOR	TYP
		GFCI	GROUND FAULT CIRCUIT INTERRUPTER	UG
		GLB CI V		UL
		GPS	GLOBAL POSITIONING SYSTEM	UNO
		GND	GROUND	UMTS
		GSM	GLOBAL SYSTEM FOR MOBILE	UPS
		HDG	HOT DIPPED GALVANIZED	W
		HDR	HANGER	W/
			HEAT AGENTILATION (AID. CONDITIONING	WD
		HVAC	HEAT/VENTILATION/AIK CONDITIONING	
		HVAC HT	HEIGHT	WP
		HVAC HT IGR	HEIGHT INTERIOR GROUND RING	WP WT

INCH INTERIOR POUND(S) LINEAR FEET LONG TERM EVOLUTION MASONRY MAXIMUM MACHINE BOLT MECHANICAL MANUFACTURER MASTER GROUND BAR MINIMUM MISCELLANEOUS METAL MANUAL TRANSFER SWITCH MICROWAVE NATIONAL ELECTRIC CODE NEWTON METERS NUMBER NUMBER NOT TO SCALE ON-CENTER OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION OPENING PRECAST CONCRETE PERSONAL COMMUNICATION SERVICES PRIMARY CONTROL UNIT PRIMARY RADIO CABINET POLARIZING PRESERVING POUNDS PER SQUARE FOOT POUNDS PER SQUARE INCH PRESSURE TREATED POWER CABINET QUANTITY RADIUS RECTIFIER REFERENCE REINFORCEMENT REQUIRED REMOTE ELECTRIC TILT RADIO FREQUENCY RIGID METALLIC CONDUIT REMOTE RADIO HEAD REMOTE RADIO UNIT RACEWAY SCHEDULE SHEET SMART INTEGRATED ACCESS DEVICE SIMILAR SPECIFICATION SQUARE STAINLESS STEEL STANDARD STEEL TEMPORARY THICKNESS TOWER MOUNTED AMPLIFIER TOE NAIL TOP OF ANTENNA TOP OF CURB TOP OF FOUNDATION TOP OF PLATE (PARAPET) TOP OF STEEL TOP OF WALL TRANSIENT VOLTAGE SURGE SUPPRESSION TYPICAL UNDERGROUND UNDERWRITERS LABORATORY UNLESS NOTED OTHERWISE UNIVERSAL MOBILE TELECOMMUNICATIONS SYSTEM UNITERRUPTIBLE POWER SYSTEM (DC POWER PLANT) VERIFIED IN FIELD WIDE WITH WOOD WEATHERPROOF WEIGHT

ABBREVIATIONS

		SIGN TYPES
TYPE	COLOR	COLOR CODE PURPOSE
INFORMATION	GREEN	"INFORMATIONAL SIGN" TO NOTIFY OTHERS OF SITE OWNERSHIP & CONTACT NUMBER AND POTENTIAL RF EXPOSURE.
NOTICE	BLUE	"NOTICE BEYOND THIS POINT" RF FIELDS BEYOND THIS POINT MAY EXCEED THE FCC GENERAL PUBLIC EXPOSURE LIMIT. OBEY ALL POSTED SIGNS AND SITE GUIDELINES FOR WORKING IN RF ENVIRONMENTS. IN ACCORDANCE WITH FEDERAL COMMUNICATIONS COMMISSION RULES ON RADIO FREQUENCY EMISSIONS 47 CFR-1.1307(b)
CAUTION	YELLOW	"CAUTION BEYOND THIS POINT" RF FIELDS BEYOND THIS POINT MAY EXCEED THE FCC GENERAL PUBLIC EXPOSURE LIMIT. OBEY ALL POSTED SIGNS AND SITE GUIDELINES FOR WORKING IN RF ENVIRONMENTS. IN ACCORDANCE WITH FEDERAL COMMUNICATIONS COMMISSION RULES ON RADIO FREQUENCY EMISSIONS 47 CFR-1.1307(b)
WARNING	ORANGE/RED	"WARNING BEYOND THIS POINT" RF FIELDS AT THIS SITE EXCEED FCC RULES FOR HUMAN EXPOSURE. FAILURE TO OBEY ALL POSTED SIGNS AND SITE GUIDELINES FOR WORKING IN RF ENVIRONMENTS COULD RESULT IN SERIOUS INJURY. IN ACCORDANCE WITH FEDERAL COMMUNICATIONS COMMISSION RULES ON RADIO FREQUENCY EMISSIONS 47 CFR-1.1307(b)

SIGN PLACEMENT:

- RF SIGNAGE PLACEMENT SHALL FOLLOW THE RECOMMENDATIONS OF AN EXISTING EME REPORT, CREATED BY A THIRD PARTY PREVIOUSLY AUTHORIZED BY DISH Wireless L.L.C.
- INFORMATION SIGN (GREEN) SHALL BE LOCATED ON EXISTING DISH Wireless L.L.C EQUIPMENT. A) IF THE INFORMATION SIGN IS A STICKER, IT SHALL BE PLACED ON EXISTING DISH Wireless L.L.C EQUIPMENT CABINET. B) IF THE INFORMATION SIGH IS A METAL SIGN IT SHALL BE PLACED ON EXISTING DISH Wireless L.L.C H-FRAME WITH A SECURE ATTACH METHOD.
- IF EME REPORT IS NOT AVAILABLE AT THE TIME OF CREATION OF CONSTRUCTION DOCUMENTS; PLEASE CONTACT DISH Wireless L.L.C. CONSTRUCTION MANAGER FOR FURTHER INSTRUCTION ON HOW TO PROCEED.

NOTES:

- 1. FOR DISH Wireless L.L.C. LOGO, SEE DISH Wireless L.L.C. DESIGN SPECIFICATIONS (PROVIDED BY DISH Wireless L.L.C.)
- 2. SITE ID SHALL BE APPLIED TO SIGNS USING "LASER ENGRAVING" OR ANY OTHER WEATHER RESISTANT METHOD (DISH Wireless L.L.C. APPROVAL REQUIRED)
- 3. TEXT FOR SIGNAGE SHALL INDICATE CORRECT SITE NAME AND NUMBER AS PER DISH Wireless L.L.C. CONSTRUCTION MANAGER RECOMMENDATIONS.
- 4. CABINET /SHELTER MOUNTING APPLICATION REQUIRES ANOTHER PLATE APPLIED TO THE FACE OF THE CABINET WITH WATER PROOF POLYURETHANE ADHESIVE
- 5. ALL SIGNS WILL BE SECURED WITH EITHER STAINLESS STEEL ZIP TIES OR STAINLESS STEEL TECH SCREWS
- 6. ALL SIGNS TO BE 8.5"x11" AND MADE WITH 0.04" OF ALUMINUM MATERIA

INFORMAT

This is an access point area with transmitting an

Obey all signs and barriers beyond t Call the DISH Wireless L.L.C. NOC at 1-

Site ID:

눷

REFEREN

Ŗ

S

THIS SIGN IS FOR REFERENCE PURPOSES ONLY

•

Transmitting Antenna(s)

Radio frequency fields beyond this po **EXCEED** the FCC Occupational expos

Obey all posted signs and site guideli working in radio frequency environme

Call the DISH Wireless L.L.C. NOC at prior to working beyond this point.

Site ID:

dish

RF SIGNAGE

Transmitting Antenna(s)

Radio frequency fields beyond this point MAY **EXCEED the FCC Occupational exposure limit.**

Obey all posted signs and site guidelines for working in radio frequency environments.

Call the DISH Wireless L.L.C. NOC at 1-866-624-6874 prior to working beyond this point.

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	DANIEL W. SMITH 44096-6 SCHAUMBURG, LL
	IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECTION OF A LICENSED PROFESSIONAL ENGINEER, TO ALTER THIS DOCUMENT. DRAWN BY: CHECKED BY: APPROVED BY: LA DZ DS RFDS REV #: 2
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SITE ACTIVITY REQUIREMENTS:

1. NOTICE TO PROCEED - NO WORK SHALL COMMENCE PRIOR TO CONTRACTOR RECEIVING A WRITTEN NOTICE TO PROCEED (NTP) AND THE ISSUANCE OF A PURCHASE ORDER. PRIOR TO ACCESSING/ENTERING THE SITE YOU MUST CONTACT THE DISH Wireless L.L.C. AND TOWER OWNER NOC & THE DISH Wireless L.L.C. AND TOWER OWNER CONSTRUCTION MANAGER.

2. "LOOK UP" - DISH Wireless L.L.C. AND TOWER OWNER SAFETY CLIMB REQUIREMENT:

THE INTEGRITY OF THE SAFETY CLIMB AND ALL COMPONENTS OF THE CLIMBING FACILITY SHALL BE CONSIDERED DURING ALL STAGES OF DESIGN, INSTALLATION, AND INSPECTION. TOWER MODIFICATION, MOUNT REINFORCEMENTS, AND/OR EQUIPMENT INSTALLATIONS SHALL NOT COMPROMISE THE INTEGRITY OR FUNCTIONAL USE OF THE SAFETY CLIMB OR ANY COMPONENTS OF THE CLIMBING FACILITY ON THE STRUCTURE. THIS SHALL INCLUDE, BUT NOT BE LIMITED TO: PINCHING OF THE WIRE ROPE, BENDING OF THE WIRE ROPE FROM ITS SUPPORTS, DIRECT CONTACT OR CLOSE PROXIMITY TO THE WIRE ROPE WHICH MAY CAUSE FRICTIONAL WEAR, IMPACT TO THE ANCHORAGE POINTS IN ANY WAY, OR TO IMPEDE/BLOCK ITS INTENDED USE. ANY COMPROMISED SAFETY CLIMB, INCLUDING EXISTING CONDITIONS MUST BE TAGGED OUT AND REPORTED TO YOUR DISH WIRE SL.C. AND DISH WIRE SL.C. AND TOWER OWNER POC OR CALL THE NOC TO GENERATE A SAFETY CLIMB MAINTENANCE AND CONTRACTOR NOTICE TICKET.

3. PRIOR TO THE START OF CONSTRUCTION, ALL REQUIRED JURISDICTIONAL PERMITS SHALL BE OBTAINED. THIS INCLUDES, BUT IS NOT LIMITED TO, BUILDING, ELECTRICAL, MECHANICAL, FIRE, FLOOD ZONE, ENVIRONMENTAL, AND ZONING. AFTER ONSITE ACTIVITIES AND CONSTRUCTION ARE COMPLETED, ALL REQUIRED PERMITS SHALL BE SATISFIED AND CLOSED OUT ACCORDING TO LOCAL JURISDICTIONAL REQUIREMENTS.

4. ALL CONSTRUCTION MEANS AND METHODS; INCLUDING BUT NOT LIMITED TO, ERECTION PLANS, RIGGING PLANS, CLIMBING PLANS, AND RESCUE PLANS SHALL BE THE RESPONSIBILITY OF THE GENERAL CONTRACTOR RESPONSIBLE FOR THE EXECUTION OF THE WORK CONTAINED HEREIN, AND SHALL MEET ANSI/ASSE A10.48 (LATEST EDITION); FEDERAL, STATE, AND LOCAL REGULATIONS; AND ANY APPLICABLE INDUSTRY CONSENSUS STANDARDS RELATED TO THE CONSTRUCTION ACTIVITIES BEING PERFORMED. ALL RIGGING PLANS SHALL ADHERE TO ANSI/ASSE A10.48 (LATEST EDITION) AND DISH WIRELS L.L.C. AND TOWER OWNER STANDARDS, INCLUDING THE REQUIRED INVOLVEMENT OF A QUALIFIED ENGINEER FOR CLASS IV CONSTRUCTION, TO CERTIFY THE SUPPORTING STRUCTURE(S) IN ACCORDANCE WITH ANSI/TIA-322 (LATEST EDITION).

5. ALL SITE WORK TO COMPLY WITH DISH WIReless L.L.C. AND TOWER OWNER INSTALLATION STANDARDS FOR CONSTRUCTION ACTIVITIES ON DISH WIREless L.L.C. AND TOWER OWNER TOWER SITE AND LATEST VERSION OF ANSI/TIA-1019-A-2012 "STANDARD FOR INSTALLATION, ALTERATION, AND MAINTENANCE OF ANTENNA SUPPORTING STRUCTURES AND ANTENNAS."

6. IF THE SPECIFIED EQUIPMENT CAN NOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE CONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION FOR APPROVAL BY DISH WIRELESS L.L.C. AND TOWER OWNER PRIOR TO PROCEEDING WITH ANY SUCH CHANGE OF INSTALLATION.

7. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS AND ORDINANCES. CONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGULATIONS.

8. THE CONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.

9. THE CONTRACTOR SHALL CONTACT UTILITY LOCATING SERVICES INCLUDING PRIVATE LOCATES SERVICES PRIOR TO THE START OF CONSTRUCTION.

10. ALL EXISTING ACTIVE SEWER, WATER, GAS, ELECTRIC AND OTHER UTILITIES WHERE ENCOUNTERED IN THE WORK, SHALL BE PROTECTED AT ALL TIMES AND WHERE REQUIRED FOR THE PROPER EXECUTION OF THE WORK, SHALL BE RELOCATED AS DIRECTED BY CONTRACTOR. EXTREME CAUTION SHOULD BE USED BY THE CONTRACTOR WHEN EXCAVATING OR DRILLING PIERS AROUND OR NEAR UTILITIES. CONTRACTOR SHALL PROVIDE SAFETY TRAINING FOR THE WORKING CREW. THIS WILL INCLUDE BUT NOT BE LIMITED TO A) FALL PROTECTION B) CONFINED SPACE C) ELECTRICAL SAFETY D) TRENCHING AND EXCAVATION E) CONSTRUCTION SAFETY PROCEDURES.

11. ALL SITE WORK SHALL BE AS INDICATED ON THE STAMPED CONSTRUCTION DRAWINGS AND DISH PROJECT SPECIFICATIONS, LATEST APPROVED REVISION.

12. CONTRACTOR SHALL KEEP THE SITE FREE FROM ACCUMULATING WASTE MATERIAL, DEBRIS, AND TRASH AT THE COMPLETION OF THE WORK. IF NECESSARY, RUBBISH, STUMPS, DEBRIS, STICKS, STONES AND OTHER REFUSE SHALL BE REMOVED FROM THE SITE AND DISPOSED OF LEGALLY.

13. ALL EXISTING INACTIVE SEWER, WATER, GAS, ELECTRIC AND OTHER UTILITIES, WHICH INTERFERE WITH THE EXECUTION OF THE WORK, SHALL BE REMOVED AND/OR CAPPED, PLUGGED OR OTHERWISE DISCONTINUED AT POINTS WHICH WILL NOT INTERFERE WITH THE EXECUTION OF THE WORK, SUBJECT TO THE APPROVAL OF DISH WIRELESS L.L.C. AND TOWER OWNER, AND/OR LOCAL UTILITIES.

14. THE CONTRACTOR SHALL PROVIDE SITE SIGNAGE IN ACCORDANCE WITH THE TECHNICAL SPECIFICATION FOR SITE SIGNAGE REQUIRED BY LOCAL JURISDICTION AND SIGNAGE REQUIRED ON INDIVIDUAL PIECES OF EQUIPMENT, ROOMS, AND SHELTERS.

15. THE SITE SHALL BE GRADED TO CAUSE SURFACE WATER TO FLOW AWAY FROM THE CARRIER'S EQUIPMENT AND TOWER AREAS.

16. THE SUB GRADE SHALL BE COMPACTED AND BROUGHT TO A SMOOTH UNIFORM GRADE PRIOR TO FINISHED SURFACE APPLICATION.

17. THE AREAS OF THE OWNERS PROPERTY DISTURBED BY THE WORK AND NOT COVERED BY THE TOWER, EQUIPMENT OR DRIVEWAY, SHALL BE GRADED TO A UNIFORM SLOPE, AND STABILIZED TO PREVENT EROSION AS SPECIFIED ON THE CONSTRUCTION DRAWINGS AND/OR PROJECT SPECIFICATIONS.

18. CONTRACTOR SHALL MINIMIZE DISTURBANCE TO EXISTING SITE DURING CONSTRUCTION. EROSION CONTROL MEASURES, IF REQUIRED DURING CONSTRUCTION, SHALL BE IN CONFORMANCE WITH THE LOCAL GUIDELINES FOR EROSION AND SEDIMENT CONTROL.

19. THE CONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT CONTRACTOR'S EXPENSE TO THE SATISFACTION OF OWNER.

20. CONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS AND RADIOS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED LOCATION.

21. CONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION. TRASH AND DEBRIS SHOULD BE REMOVED FROM SITE ON A DAILY BASIS.

22. NO FILL OR EMBANKMENT MATERIAL SHALL BE PLACED ON FROZEN GROUND. FROZEN MATERIALS, SNOW OR ICE SHALL NOT

BE PLACED IN ANY FILL OR EMBANKMENT.

GENERAL NOTES:

1.FOR THE PURPOSE OF CONSTRUCTION DRAWING, THE FOLLOWING DEFINITIONS SHALL APPLY:

CONTRACTOR: GENERAL CONTRACTOR RESPONSIBLE FOR CONSTRUCTION

CARRIER: DISH Wireless L.L.C.

STRUCTURE OWNER: SEE T-1 FOR INFO

2. THESE DRAWINGS HAVE BEEN PREPARED USING STANDARDS OF PROFESSIONAL CARE AND COMPLETENESS NORMALLY EXERCISED UNDER SIMILAR CIRCUMSTANCES BY REPUTABLE ENGINEERS IN THIS OR SIMILAR LOCALITIES. IT IS ASSUMED THAT THE WORK DEPICTED WILL BE PERFORMED BY AN EXPERIENCED CONTRACTOR AND/OR WORKPEOPLE WHO HAVE A WORKING KNOWLEDGE OF THE APPLICABLE CODE STANDARDS AND REQUIREMENTS AND OF INDUSTRY ACCEPTED STANDARD GOOD PRACTICE. AS NOT EVERY CONDITION OR ELEMENT IS (OR CAN BE) EXPLICITLY SHOWN ON THESE DRAWINGS, THE CONTRACTOR SHALL USE INDUSTRY ACCEPTED STANDARD GOOD PRACTICE FOR MISCELLANEOUS WORK NOT EXPLICITLY SHOWN.

3. THESE DRAWINGS REPRESENT THE FINISHED STRUCTURE. THEY DO NOT INDICATE THE MEANS OR METHODS OF CONSTRUCTION. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR THE CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES. THE CONTRACTOR SHALL PROVIDE ALL MEASURES NECESSARY FOR PROTECTION OF LIFE AND PROPERTY DURING CONSTRUCTION. SUCH MEASURES SHALL INCLUDE, BUT NOT BE LIMITED TO, BRACING, FORMWORK, SHORING, ETC. SITE VISITS BY THE ENGINEER OR HIS REPRESENTATIVE WILL NOT INCLUDE INSPECTION OF THESE ITEMS AND IS FOR STRUCTURAL OBSERVATION OF THE FINISHED STRUCTURE ONLY.

4. NOTES AND DETAILS IN THE CONSTRUCTION DRAWINGS SHALL TAKE PRECEDENCE OVER GENERAL NOTES AND TYPICAL DETAILS. WHERE NO DETAILS ARE SHOWN, CONSTRUCTION SHALL CONFORM TO SIMILAR WORK ON THE PROJECT, AND/OR AS PROVIDED FOR IN THE CONTRACT DOCUMENTS. WHERE DISCREPANCIES OCCUR BETWEEN PLANS, DETAILS, GENERAL NOTES, AND SPECIFICATIONS, THE GREATER, MORE STRICT REQUIREMENTS, SHALL GOVERN. IF FURTHER CLARIFICATION IS REQUIRED CONTACT THE ENGINEER OF RECORD.

5. SUBSTANTIAL EFFORT HAS BEEN MADE TO PROVIDE ACCURATE DIMENSIONS AND MEASUREMENTS ON THE DRAWINGS TO ASSIST IN THE FABRICATION AND/OR PLACEMENT OF CONSTRUCTION ELEMENTS BUT IT IS THE SOLE RESPONSIBILITY OF THE CONTRACTOR TO FIELD VERIFY THE DIMENSIONS, MEASUREMENTS, AND/OR CLEARANCES SHOWN IN THE CONSTRUCTION DRAWINGS PRIOR TO FABRICATION OR CUTTING OF ANY NEW OR EXISTING CONSTRUCTION ELEMENTS. IF IT IS DETERMINED THAT THERE ARE DISCREPANCIES AND/OR CONFLICTS WITH THE CONSTRUCTION DRAWINGS THE ENGINEER OF RECORD IS TO BE NOTIFIED AS SOON AS POSSIBLE.

6. PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING CONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF CARRIER POC AND TOWER OWNER.

7. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS AND ORDINANCES. CONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGULATIONS.

8. UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT, APPURTENANCES AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS.

9. THE CONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.

10. IF THE SPECIFIED EQUIPMENT CAN NOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE CONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION FOR APPROVAL BY THE CARRIER AND TOWER OWNER PRIOR TO PROCEEDING WITH ANY SUCH CHANGE OF INSTALLATION.

11. CONTRACTOR IS TO PERFORM A SITE INVESTIGATION, BEFORE SUBMITTING BIDS, TO DETERMINE THE BEST ROUTING OF ALL CONDUITS FOR POWER, AND TELCO AND FOR GROUNDING CABLES AS SHOWN IN THE POWER, TELCO, AND GROUNDING PLAN DRAWINGS.

12. THE CONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT CONTRACTOR'S EXPENSE TO THE SATISFACTION OF DISH Wireless L.L.C. AND TOWER OWNER

13. CONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED LOCATION.

14. CONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION. TRASH AND DEBRIS SHOULD BE REMOVED FROM SITE ON A DAILY BASIS.

DSCAPING AND STRUCTURES. ANY SH Wireless L.L.C. AND TOWER OWNER H AS COAXIAL CABLES AND OTHER HE OWNER'S DESIGNATED LOCATION.

CONCRETE, FOUNDATIONS, AND REINFORCING STEEL:

ALL CONCRETE WORK SHALL BE IN ACCORDANCE WITH THE ACI 301, ACI 318, ACI 336, ASTM A184, ASTM A185 AND THE DESIGN AND CONSTRUCTION SPECIFICATION FOR CAST-IN-PLACE CONCRETE.

2 UNLESS NOTED OTHERWISE, SOIL BEARING PRESSURE USED FOR DESIGN OF SLABS AND FOUNDATIONS IS ASSUMED TO BE 1000 psf.

ALL CONCRETE SHALL HAVE A MINIMUM COMPRESSIVE STRENGTH (f'c) OF 3000 psi AT 28 DAYS, UNLESS NOTED OTHERWISE. NO 3. MORE THAN 90 MINUTES SHALL ELAPSE FROM BATCH TIME TO TIME OF PLACEMENT UNLESS APPROVED BY THE ENGINEER OF RECORD. TEMPERATURE OF CONCRETE SHALL NOT EXCEED 90'F AT TIME OF PLACEMENT.

CONCRETE EXPOSED TO FREEZE-THAW CYCLES SHALL CONTAIN AIR ENTRAINING ADMIXTURES. AMOUNT OF AIR ENTRAINMENT TO BE BASED ON SIZE OF AGGREGATE AND F3 CLASS EXPOSURE (VERY SEVERE). CEMENT USED TO BE TYPE II PORTLAND CEMENT WITH A MAXIMUM WATER-TO-CEMENT RATIO (W/C) OF 0.45.

ALL STEEL REINFORCING SHALL CONFORM TO ASTM A615. ALL WELDED WIRE FABRIC (WWF) SHALL CONFORM TO ASTM A185. ALL SPLICES SHALL BE CLASS "B" TENSION SPLICES, UNLESS NOTED OTHERWISE. ALL HOOKS SHALL BE STANDARD 90 DEGREE HOOKS, UNLESS NOTED OTHERWISE. YIELD STRENGTH (Fy) OF STANDARD DEFORMED BARS ARE AS FOLLOWS:

#4 BARS AND SMALLER 40 ksi

#5 BARS AND LARGER 60 ksi

THE FOLLOWING MINIMUM CONCRETE COVER SHALL BE PROVIDED FOR REINFORCING STEEL UNLESS SHOWN OTHERWISE ON DRAWINGS:

- CONCRETE CAST AGAINST AND PERMANENTLY EXPOSED TO EARTH 3"
- CONCRETE EXPOSED TO EARTH OR WEATHER:
- #6 BARS AND LARGER 2"
- #5 BARS AND SMALLER 1-1/2"
- · CONCRETE NOT EXPOSED TO EARTH OR WEATHER:
- SLAB AND WALLS 3/4"
- BEAMS AND COLUMNS 1-1/2"

A TOOLED EDGE OR A 3/4" CHAMFER SHALL BE PROVIDED AT ALL EXPOSED EDGES OF CONCRETE, UNLESS NOTED OTHERWISE, IN ACCORDANCE WITH ACI 301 SECTION 4.2.4.

ELECTRICAL INSTALLATION NOTES:

ALL ELECTRICAL WORK SHALL BE PERFORMED IN ACCORDANCE WITH THE PROJECT SPECIFICATIONS, NEC AND ALL APPLICABLE FEDERAL, STATE, AND LOCAL CODES/ORDINANCES.

CONDUIT ROUTINGS ARE SCHEMATIC. CONTRACTOR SHALL INSTALL CONDUITS SO THAT ACCESS TO EQUIPMENT IS NOT BLOCKED AND TRIP HAZARDS ARE ELIMINATED.

3. WIRING, RACEWAY AND SUPPORT METHODS AND MATERIALS SHALL COMPLY WITH THE REQUIREMENTS OF THE NEC.

ALL CIRCUITS SHALL BE SEGREGATED AND MAINTAIN MINIMUM CABLE SEPARATION AS REQUIRED BY THE NEC.

4.1. ALL EQUIPMENT SHALL BEAR THE UNDERWRITERS LABORATORIES LABEL OF APPROVAL, AND SHALL CONFORM TO REQUIREMENT OF THE NATIONAL ELECTRICAL CODE.

ALL OVERCURRENT DEVICES SHALL HAVE AN INTERRUPTING CURRENT RATING THAT SHALL BE GREATER THAN THE SHORT CIRCUIT CURRENT TO WHICH THEY ARE SUBJECTED, 22,000 AIC MINIMUM. VERIFY AVAILABLE SHORT CIRCUIT CURRENT DOES NOT EXCEED THE RATING OF ELECTRICAL EQUIPMENT IN ACCORDANCE WITH ARTICLE 110.24 NEC OR THE MOST CURRENT ADOPTED CODE PRE THE GOVERNING JURISDICTION.

EACH END OF EVERY POWER PHASE CONDUCTOR, GROUNDING CONDUCTOR, AND TELCO CONDUCTOR OR CABLE SHALL BE LABELED WITH COLOR-CODED INSULATION OR ELECTRICAL TAPE (3M BRAND, 1/2" PLASTIC ELECTRICAL TAPE WITH UV PROTECTION, OR EQUAL). THE IDENTIFICATION METHOD SHALL CONFORM WITH NEC AND OSHA.

ALL ELECTRICAL COMPONENTS SHALL BE CLEARLY LABELED WITH LAMICOID TAGS SHOWING THEIR RATED VOLTAGE, PHASE CONFIGURATION, WRE CONFIGURATION, POWER OR AMPACITY RATING AND BRANCH CIRCUIT ID NUMBERS (i.e. PANEL BOARD AND CIRCUIT ID'S).

7. PANEL BOARDS (ID NUMBERS) SHALL BE CLEARLY LABELED WITH PLASTIC LABELS.

8 TIE WRAPS ARE NOT ALLOWED

ALL POWER AND EQUIPMENT GROUND WIRING IN TUBING OR CONDUIT SHALL BE SINGLE COPPER CONDUCTOR (#14 OR LARGER) 9 WITH TYPE THHW, THWN, THWN-2, XHHW, XHHW-2, THW, THW-2, RHW, OR RHW-2 INSULATION UNLESS OTHERWISE SPECIFIED.

SUPPLEMENTAL EQUIPMENT GROUND WIRING LOCATED INDOORS SHALL BE SINGLE COPPER CONDUCTOR (#6 OR LARGER) WITH 10. TYPE THHW, THWN, THWN-2, XHHW, XHHW-2, THW, THW-2, RHW, OR RHW-2 INSULATION UNLESS OTHERWISE SPECIFIED.

POWER AND CONTROL WIRING IN FLEXIBLE CORD SHALL BE MULTI-CONDUCTOR, TYPE SOOW CORD (#14 OR LARGER) UNLESS OTHERWISE SPECIFIED.

POWER AND CONTROL WIRING FOR USE IN CABLE TRAY SHALL BE MULTI-CONDUCTOR. TYPE TC CABLE (#14 OR LARGER), WITH 12. TYPE THHW, THWN, THWN-2, XHHW, XHHW-2, THW, THW-2, RHW, OR RHW-2 INSULATION UNLESS OTHERWISE SPECIFIED.

13 ALL POWER AND GROUNDING CONNECTIONS SHALL BE CRIMP-STYLE, COMPRESSION WIRE LUGS AND WIRE NUTS BY THOMAS AND BETTS (OR EQUAL). LUGS AND WIRE NUTS SHALL BE RATED FOR OPERATION NOT LESS THAN 75° C (90° C IF AVAILABLE).

14. RACEWAY AND CABLE TRAY SHALL BE LISTED OR LABELED FOR ELECTRICAL USE IN ACCORDANCE WITH NEMA, UL, ANSI/IEEE AND NEC.

15 ELECTRICAL METALLIC TUBING (EMT), INTERMEDIATE METAL CONDUIT (IMC), OR RIGID METAL CONDUIT (RMC) SHALL BE USED FOR EXPOSED INDOOR LOCATIONS.

ELECTRICAL METALLIC TUBING (EMT) OR METAL-CLAD CABLE (MC) SHALL BE USED FOR CONCEALED INDOOR LOCATIONS. 16.

SCHEDULE 40 PVC UNDERGROUND ON STRAIGHTS AND SCHEDULE 80 PVC FOR ALL ELBOWS/90s AND ALL APPROVED ABOVE 17 GRADE PVC CONDUIT.

LIQUID-TIGHT FLEXIBLE METALLIC CONDUIT (LIQUID-TITE FLEX) SHALL BE USED INDOORS AND OUTDOORS, WHERE VIBRATION OCCURS OR FLEXIBILITY IS NEEDED.

CONDUIT AND TUBING FITTINGS SHALL BE THREADED OR COMPRESSION-TYPE AND APPROVED FOR THE LOCATION USED. SET SCREW FITTINGS ARE NOT ACCEPTABLE.

CABINETS, BOXES AND WIRE WAYS SHALL BE LABELED FOR ELECTRICAL USE IN ACCORDANCE WITH NEMA, UL, ANSI/IEEE AND 20. THE NEC.

21 WREWAYS SHALL BE METAL WITH AN ENAMEL FINISH AND INCLUDE A HINGED COVER, DESIGNED TO SWING OPEN DOWNWARDS (WIREMOLD SPECMATE WIREWAY).

22. SLOTTED WIRING DUCT SHALL BE PVC AND INCLUDE COVER (PANDUIT TYPE E OR EQUAL).

23. CONDUITS SHALL BE FASTENED SECURELY IN PLACE WITH APPROVED NON-PERFORATED STRAPS AND HANGERS. EXPLOSIVE DEVICES (i.e. POWDER-ACTUATED) FOR ATTACHING HANGERS TO STRUCTURE WILL NOT BE PERMITTED. CLOSELY FOLLOW THE LINES OF THE STRUCTURE, MAINTAIN CLOSE PROXIMITY TO THE STRUCTURE AND KEEP CONDUITS IN TIGHT ENVELOPES. CHANGES IN DIRECTION TO ROUTE AROUND OBSTACLES SHALL BE MADE WITH CONDUIT OUTLET BODIES. CONDUIT SHALL BE INSTALLED IN A NEAT AND WORKMANLIKE MANNER. PARALLEL AND PERPENDICULAR TO STRUCTURE WALL AND CEILING LINES. ALL CONDUIT SHALL BE FISHED TO CLEAR OBSTRUCTIONS. ENDS OF CONDUITS SHALL BE TEMPORARILY CAPPED FLUSH TO FINISH GRADE TO PREVENT CONCRETE, PLASTER OR DIRT FROM ENTERING. CONDUITS SHALL BE RIGIDLY CLAMPED TO BOXES BY GALVANIZED MALLEABLE IRON BUSHING ON INSIDE AND GALVANIZED MALLEABLE IRON LOCKNUT ON OUTSIDE AND INSIDE.

EQUIPMENT CABINETS, TERMINAL BOXES, JUNCTION BOXES AND PULL BOXES SHALL BE GALVANIZED OR EPOXY-COATED SHEET 24. STEEL. SHALL MEET OR EXCEED UL 50 AND BE RATED NEMA 1 (OR BETTER) FOR INTERIOR LOCATIONS AND NEMA 3 (OR BETTER) FOR EXTERIOR LOCATIONS.

METAL RECEPTACLE, SWITCH AND DEVICE BOXES SHALL BE GALVANIZED, EPOXY-COATED OR NON-CORRODING: SHALL MEET OR 25 EXCEED UL 514A AND NEMA OS 1 AND BE RATED NEMA 1 (OR BETTER) FOR INTERIOR LOCATIONS AND WEATHER PROTECTED (WP OR BETTER) FOR EXTERIOR LOCATIONS.

NONMETALLIC RECEPTACLE, SWITCH AND DEVICE BOXES SHALL MEET OR EXCEED NEMA OS 2 (NEWEST REVISION) AND BE RATED 26 NEMA 1 (OR BETTER) FOR INTERIOR LOCATIONS AND WEATHER PROTECTED (WP OR BETTER) FOR EXTERIOR LOCATIONS.

THE CONTRACTOR SHALL NOTIFY AND OBTAIN NECESSARY AUTHORIZATION FROM THE CARRIER AND/OR DISH Wireless L.L.C. AND 27 TOWER OWNER BEFORE COMMENCING WORK ON THE AC POWER DISTRIBUTION PANELS.

28 THE CONTRACTOR SHALL PROVIDE NECESSARY TAGGING ON THE BREAKERS, CABLES AND DISTRIBUTION PANELS IN ACCORDANCE WITH THE APPLICABLE CODES AND STANDARDS TO SAFEGUARD LIFE AND PROPERTY.

- 29. INSTALL LAMICOID LABEL ON THE METER CENTER TO SHOW "DISH Wireless L.L.C.".
- 30. ALL EMPTY/SPARE CONDUITS THAT ARE INSTALLED ARE TO HAVE A METERED MULE TAPE PULL CORD INSTALLED.

GROUNDING NOTES:

1. ALL GROUND ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATION, RADIO, LIGHTNING PROTECTION AND AC POWER GES'S) SHALL BE BONDED TOGETHER AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS IN ACCORDANCE WITH THE NEC.

2. THE CONTRACTOR SHALL PERFORM IEEE FALL-OF-POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR GROUND ELECTRODE SYSTEMS, THE CONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 5 OHMS OR LESS.

3. THE CONTRACTOR IS RESPONSIBLE FOR PROPERLY SEQUENCING GROUNDING AND UNDERGROUND CONDUIT INSTALLATION AS TO PREVENT ANY LOSS OF CONTINUITY IN THE GROUNDING SYSTEM OR DAMAGE TO THE CONDUIT AND PROVIDE TESTING RESULTS.

4. METAL CONDUIT AND TRAY SHALL BE GROUNDED AND MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTINGS OR BY BONDING ACROSS THE DISCONTINUITY WITH #6 COPPER WIRE UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.

5. METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO BTS EQUIPMENT.

6. EACH CABINET FRAME SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRES, #6 STRANDED COPPER OR LARGER FOR INDOOR BTS; #2 BARE SOLID TINNED COPPER FOR OUTDOOR BTS.

7. CONNECTIONS TO THE GROUND BUS SHALL NOT BE DOUBLED UP OR STACKED BACK TO BACK CONNECTIONS ON OPPOSITE SIDE OF THE GROUND BUS ARE PERMITTED.

8. ALL EXTERIOR GROUND CONDUCTORS BETWEEN EQUIPMENT/GROUND BARS AND THE GROUND RING SHALL BE #2 SOLID TINNED COPPER UNLESS OTHERWISE INDICATED.

9. ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.

10. USE OF 90° BENDS IN THE PROTECTION GROUNDING CONDUCTORS SHALL BE AVOIDED WHEN 45° BENDS CAN BE ADEQUATELY SUPPORTED.

11. EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE.

12. ALL GROUND CONNECTIONS ABOVE GRADE (INTERIOR AND EXTERIOR) SHALL BE FORMED USING HIGH PRESS CRIMPS.

13. COMPRESSION GROUND CONNECTIONS MAY BE REPLACED BY EXOTHERMIC WELD CONNECTIONS.

14. ICE BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO THE BRIDGE AND THE TOWER GROUND BAR.

15. APPROVED ANTIOXIDANT COATINGS (i.e. CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.

16. ALL EXTERIOR GROUND CONNECTIONS SHALL BE COATED WITH A CORROSION RESISTANT MATERIAL.

17. MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RING, IN ACCORDANCE WITH THE NEC.

18. BOND ALL METALLIC OBJECTS WITHIN 6 ft OF MAIN GROUND RING WITH (1) #2 BARE SOLID TINNED COPPER GROUND CONDUCTOR.

19. GROUND CONDUCTORS USED FOR THE FACILITY GROUNDING AND LIGHTNING PROTECTION SYSTEMS SHALL NOT BE ROUTED THROUGH METALLIC OBJECTS THAT FORM A RING AROUND THE CONDUCTOR, SUCH AS METALLIC CONDUITS, METAL SUPPORT CLIPS OR SLEEVES THROUGH WALLS OR FLOORS. WHEN IT IS REQUIRED TO BE HOUSED IN CONDUIT TO MEET CODE REQUIREMENTS OR LOCAL CONDITIONS, NON-METALLIC MATERIAL SUCH AS PVC CONDUIT SHALL BE USED. WHERE USE OF METAL CONDUIT IS UNAVOIDABLE (i.e., NONMETALLIC CONDUIT PROHIBITED BY LOCAL CODE) THE GROUND CONDUCTOR SHALL BE BONDED TO EACH END OF THE METAL CONDUIT.

20. ALL GROUNDS THAT TRANSITION FROM BELOW GRADE TO ABOVE GRADE MUST BE #2 BARE SOLID TINNED COPPER IN 3/4" NON-METALLIC, FLEXIBLE CONDUIT FROM 24" BELOW GRADE TO WITHIN 3" TO 6" OF CAD-WELD TERMINATION POINT. THE EXPOSED END OF THE CONDUIT MUST BE SEALED WITH SILICONE CAULK. (ADD TRANSITIONING GROUND STANDARD DETAIL AS WELL).

21. BUILDINGS WHERE THE MAIN GROUNDING CONDUCTORS ARE REQUIRED TO BE ROUTED TO GRADE, THE CONTRACTOR SHALL ROUTE TWO GROUNDING CONDUCTORS FROM THE ROOFTOP, TOWERS, AND WATER TOWERS GROUNDING RING, TO THE EXISTING GROUNDING SYSTEM, THE GROUNDING CONDUCTORS SHALL NOT BE SMALLER THAN 2/0 COPPER. ROOFTOP GROUNDING RING SHALL BE BONDED TO THE EXISTING GROUNDING SYSTEM, THE BUILDING STEEL COLUMNS, LIGHTNING PROTECTION SYSTEM, AND BUILDING MAIN WATER LINE (FERROUS OR NONFERROUS METAL PIPING ONLY). DO NOT ATTACH GROUNDING TO FIRE SPRINKLER SYSTEM PIPES.

STRUCTURAL NOTES:

APPLICABLE CODES

 DESIGN & CONSTRUCTION OF ALL WORK SHALL CONFORM TO THE FOLLOWING CODES: 2018 WISCONSIN COMMERCIAL BUILDING CODE TIA-222-H

DESIGN LOADS:

WIND LOAD: 107 MPH BASIC DESIGN WIND SPEED PER TIA-222-H

GENERAL NOTES

- 1. THE CONTRACTOR SHALL BE RESPONSIBLE FOR FOLLOWING ALL LAWS, REGULATIONS, AND RULES SET FORTH BY FEDERAL, STATE, AND LOCAL AUTHORITIES WITH JURISDICTION OVER THE PROJECT. THIS RESPONSIBILITY IS IN EFFECT REGARDLESS OF WHETHER THE LAW, ORDINANCE, REGULATION OR RULE IS MENTIONED IN THESE SPECIFICATIONS.
- 2. ALL WORK SHALL BE COMPLETED AS INDICATED ON THE DRAWINGS, PROJECT SPECIFICATIONS, AND THE CONSTRUCTION CONTRACT DOCUMENTS.
- 3. THE CONTRACTOR SHALL HAVE AND MAINTAIN A VALID CONTRACTOR'S LICENSE FOR THE LOCATION IN WHICH THE WORK IS TO BE PERFORMED. FOR JURISDICTIONS THAT LICENSE INDIVIDUAL TRADES, THE TRADESMAN OR SUBCONTRACTOR PERFORMING THOSE TRADES SHALL BE LICENSED.
- 4. FOLLOW ALL APPLICABLE RULES AND REGULATIONS OF THE OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION (OSHA) AND STATE LAW AS DEFINED IN THE FEDERAL OCCUPATIONAL SAFETY AND HEALTH ACT.
- 5. PRIOR TO THE SUBMISSION OF THE BID, THE CONTRACTOR SHALL VISIT THE JOB SITE, VERIFY ALL DIMENSIONS AND BECOME FAMILIAR WITH THE FIELD CONDITIONS. ANY DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE PROJECT MANAGER.
- 6. DRAWING PLANS SHALL NOT BE SCALED.
- THE CONTRACTOR SHALL NOT PROCEED WITH ANY WORK NOT CLEARLY IDENTIFIED ON THE DRAWINGS WITHOUT THE PRIOR WRITTEN APPROVAL OF THE PROJECT MANAGER.
- 8. THE CONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER RECOMMENDATIONS UNLESS SPECIFICALLY OTHERWISE NOTED.
- 9. ALL MEANS AND METHODS OF CONSTRUCTION DEALING WITH TOWER CONSTRUCTION AND SAFETY, STEEL ERECTION, EXCAVATIONS, TRENCHING, SCAFFOLDING, FORMWORK, ELECTRICAL, AND WORK IN CONFINED SPACES ARE THE SOLE RESPONSIBILITY OF THE CONTRACTOR.
- 10. THE CONTRACTOR SHALL BE RESPONSIBLE FOR INITIATING, MAINTAINING, AND SUPERVISING ALL SAFETY PRECAUTIONS AND PROGRAMS IN CONNECTION WITH THE WORK.
- 11. THE CONTRACTOR SHALL BE EXPERIENCED IN THE PERFORMANCE OF WORK SIMILAR TO THAT DESCRIBED HEREIN. BY ACCEPTANCE OF THIS ASSIGNMENT, THE CONTRACTOR IS ATTESTING THAT HE DOES HAVE SUFFICIENT EXPERIENCE AND ABILITY AND THAT HE IS KNOWLEDGEABLE OF THE WORK TO BE PERFORMED.
- 12. THE CONTRACTOR SHALL PROVIDE SUFFICIENT TEMPORARY BRACING AND/OR SHORING OF ALL STRUCTURAL AND NON-STRUCTURAL ELEMENTS DURING CONSTRUCTION UNTIL ALL STRUCTURAL ELEMENTS HAVE BEEN PROPERLY INSTALLED.
- 13. INCORRECTLY FABRICATED, DAMAGED, OR OTHERWISE MISFITTING OR NONCONFORMING MATERIALS SHALL BE REPORTED TO THE PROJECT MANAGER AND ENGINEER, AND SHALL REQUIRE APPROVAL PRIOR TO PERFORMING ANY REMEDIAL OR CORRECTIVE ACTION.

STRUCTURAL STEEL NOTES:

- 1. STRUCTURAL STEEL MATERIALS CONFORM TO THE LATEST EDITION OF APPLICABLE STANDARDS AND TO ALL APPLICABLE CODES AND REQUIREMENTS OF LOCAL AUTHORITIES HAVING JURISDICTION, WHICHEVER IS MORE STRINGENT. ALL STRUCTURAL STEEL SHALL BE IN ACCORDANCE WITH THE LATEST APPLICABLE REQUIREMENTS OF AISC, ASTM, ACI, CRSI, AWS AND ALL OTHER APPLICABLE STANDARDS
- ALL NEW STRUCTURAL STEEL SHALL CONFORM TO THE FOLLOWING, UNLESS NOTED OTHERWISE ON THE DRAWINGS: ASTM A36 (Fy = 36 KSI) M-SHAPES, S-SHAPES, ANGLES, PLATES (U.N.O.) ASTM A992 (Fy = 50 KSI) W-SHAPES, CHANNELS (U.N.O.) ASTM A500 Gr C (Fy = 50 KSI) ROUND AND SQUARE HSS
- 3. STEEL PIPE SHALL COMPLY WITH ASTM A53 GRADE B. MAY BE SUBSTITUTED WITH ASTM 500 GRADE C (ROUND HSS)
- ALL STRUCTURAL STEEL SHALL BE HOT DIPPED GALVANIZED IN ACCORDANCE WITH ASTM A153 AND A123, INCLUDING CONNECTION HARDWARE (BOLTS, WASHERS, NUTS, AND PINS), PLATES, SPACERS, AND FILLERS.
- 5. CONNECTIONS:
 - A. CONTRACTOR SHALL PROVIDE ALL HARDWARE REQUIRED TO COMPLETE FIELD ERECTION OF STRUCTURE AS INDICATED BY CONTRACT DOCUMENTS OR THESE SPECIFICATIONS.
 - B. HIGH STRENGTH THREADED FASTENERS SHALL BE INSTALLED IN ACCORDANCE WITH AISC SPECIFICATIONS FOR STRUCTURAL JOINTS USING ASTM A-325 BOLTS. USE A-325N BEARING-TYPE CONNECTION BOLTS UNLESS NOTED OTHERWISE.
 - C. GRATING AND PLATES SHALL BE FASTENED WITH SADDLE CLIPS. THE NECESSARY HOLES TO COMPLETE ALL PHASES OF CONSTRUCTION SHALL BE PROVIDED AND CALLED OUT ON THE APPROVED SHOP DRAWINGS. ALL HOLES SHALL BE DRILLED OR PUNCHED PERPENDICULAR TO METAL SURFACES, FLAME CUT OR BURNED HOLES WILL NOT BE PERMITTED.
 - D. ALL UNFINISHED THREADED FASTENERS SHALL COMPLY WITH ASTM A-307, GRADE A, REGULAR LOW-CARBON STEEL BOLTS AND NUTS WITH HEXAGONAL HEADS.
 - E. ALL HIGH STRENGTH THREADED FASTENERS SHALL BE HEAVY HEXAGONAL BOLTS AND NUTS WITH HARDENED WASHERS, ALL FROM QUENCHED AND TEMPERED MEDIUM CARBON STEEL COMPLYING WITH ASTM A-325.

STRUCTURAL ANALYSIS REPORT

STRUCTURE: ROOFTOP

PREPARED FOR: DISH Wireless

CARRIER: DISH Wireless

SITE NUMBER : MWMKE00116B

SITE LOCATION: 314 6th Street Racine, WI 53403 N42.72684, W87.784674

DATE: June 2, 2022

RESULTS PASS (MAX STRESS RATIO: 64.9%)

Jul 7 2022

Barbara T. Kotecki, P.E.

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Project Number: 2021.0030.0004

Summary

The structural analysis was performed by Fullerton, as requested by the client, to determine the conformance of existing structure with the governing 2018 Wisconsin Commercial Building Code and the industry standard, TIA-222-H (Structural Standards for Steel Antenna Supporting Structures, Antennas, and Small Wind Turbine Support Structures). The analysis considers the relevant structural properties, the existing and proposed appurtenances, and the required loading criteria.

Conclusion

Component	% Capacity	Pass / Fail
New Wall Mounts (Sector Alpha)	56.1%	PASS
New Wall Mounts (Sector Beta)	64.9%	PASS
New Wall Mounts (Sector Gamma)	51.6%	PASS
New Equipment Platform (Sector Gamma)	36.5%	PASS
Structural Rating (max from all comp	PASS	

Sources

The following documents for the existing structure were made available for our structural analysis.

Reference Document	Date
RFDS Revision 2 provided by Dish	08/31/2021
Construction Drawings by Fullerton Engineering Consultants	Latest Version
Field Investigation Report by Fullerton Engineering	10/04/2021
Site Visit Photos	10/01/2021, 12/13/2021

Appurtenance Loading Schedule

EQUIPMENT				
ELEVATION (Ft)	QTY.	MANUFACTURER/MODEL		
	1	(N) Commscope FFVV-65B-R2		
59'-0"	1	(N) Fujitsu TA08025-B605 RRH Unit		
	1	(N) Fujitsu TA08025-B604 RRH Unit		
	1	(N) Raycap RDIDC-3045-PF-48 OVP		
Rooftop	1	(N) Charles HEX CUBE-PM639155N4 (74"H x 32"W x 32"D – 1067.14#)		
	1	(N) Raycap PPC RDIAC-2465-P-240-MTS		
	1	(N) Charles CFIT-PF2020DSH1 Fiber Telco Enclosure		

(E) denotes existing loading

(N) denotes proposed loading

- New appurtenances will be mounted on new wall mounts (Site Pro 1 Part# SBWM) in Sector Alpha and Gamma and new wall mount angles on Sector Beta.
- New equipment cabinet will be installed on new steel equipment platform attached to existing parapet wall and elevated roof wall..

Assumptions

This analysis is based on the theoretical capacity of the members and is not a condition assessment of the tower. The analysis is based solely on the information supplied, and the results, in turn, are only as accurate as data extracted from this information. Fullerton has been instructed by the client to assume the information supplied is accurate, and Fullerton has made no independent determination of its accuracy. The exception to the previous statement is if Fullerton has been contracted by the client to provide an independent structural mapping report of the tower and related appurtenances, in which case Fullerton has made an independent determination of the accuracy of the information resulting from the mapping report.

- Member sizes and geometry are considered accurate as supplied. The material grade is as per data supplied and/or as assumed and stated in the materials section.
- The existing structure is assumed to have been properly maintained in accordance with the TIA/EIA standard and/or its original manufacturer's recommendations. The existing structure is assumed to be in good condition with no structural defects and with no deterioration to its member capacities.
- The antenna configuration is as supplied and/or stated in the analysis section. It is assumed to be complete and accurate. All antennas, mounts, remote radios, cables, and cable supports are assumed to be properly installed and supported as per the manufacturer's requirements.
- The antennas, mounts, remote radios, cables, and cable supports, and lines stated in the appurtenance loading schedule represent Fullerton's understanding of the overall antenna configuration. If the actual configuration is different than above, then this analysis is invalid. Please refer to this report for the projected wind areas used in the calculations for antennas and mounts. If variations or discrepancies are identified, please inform Fullerton.
- Some assumptions are made regarding antenna and mount sizes and their projected areas based on a best interpretation of the data supplied and a best knowledge of antenna type and industry practice.
- All welds and connections are assumed to develop at least the member capacity, unless determined otherwise and explicitly stated in this report.
- All prior structural modifications, if any, are assumed to be as per date supplied/ available, to be properly installed and to be fully effective.

Scope and Limitations

The engineering services rendered by Fullerton Engineering Consultants, LLC (Fullerton) in connection with this structural analysis are limited to an analysis of the structure, size, and capacity of its members. Fullerton does not analyze the fabrication, including welding and connection capacities, except as included in this report.

The information and conclusions contained in this report were determined by application of the current engineering standards and analysis procedures and formulae, and Fullerton assumes no obligation to revise any of the information or conclusions contained in this report in the event such engineering and analysis procedures and formulae are hereafter modified or revised.

Fullerton makes no warranties, expressed, or implied in connection with this report and disclaims any liability arising from original design, material, fabrication, and erection deficiencies or the "as-built" condition of this tower.

Installation procedures are not within the scope of this report and should be performed and evaluated by a competent tower erection contractor.

Structural Calculations

Fullerton Engineering Consultants, LLC.

Analysis and Design Criteria		
Type of Structure	Rooftop 🗸	
Elevation of Antenna Centerline Above Ground	z := 59f	
Structure Height Above Grade	h := 49.25f	
Mid-Point of Structure	$h_{mid} := \frac{h}{2}$	
Mean Elevation of Structure above Sea Level	$Z_{S} := 624.28$ ft	
Risk Category		ANSI/TIA-222-H: Table 2-1
Basic Wind Speed (no ice): 3-Second Gust	<mark></mark>	ANSI/TIA-222-H: ANNEX B
Basic Wind Speed (with ice): 3-Second Gust	V _i := 40 mph	ANSI/TIA-222-H: ANNEX B
Basic Wind Speed (maintenance): 3-Second Gust	V _m := 30 mph	ANSI/TIA-222-H: Section 16.3
Ice Thickness	t _i := 1.5in	ANSI/TIA-222-H: ANNEX B
Exposure Category	CV	ANSI/TIA-222-H: Section 2.6.5.1.2
Topographic Category	1	ANSI/TIA-222-H: Section 2.6.6.2.1
Height of Crest Above Surrounding Terrain	<mark></mark>	
Gust Effect Factor	G _h := 1	ANSI/TIA-222-H, Section 16.6

Fullerton Engineering Consultants, LLC.

	F	
	1	

b		
Ground Elevation Factor	$K_{e} = 0.98$	ANSI/TIA-222-H: Section 2.6.8
Wind Direction Probability Factor	$K_{d} = 0.95$	ANSI/TIA-222-H: Table 2-2
Velocity Pressure Coefficient	$K_{Z} = 1.13$	ANSI/TIA-222-H: Section 2.6.5.2
Topographic Factor	$K_{zt} = 1$	ANSI/TIA-222-H: Section 2.6.6.2.1
Rooftop Wind Speed-Up Factor	$K_{S} = 1$	ANSI/TIA-222-H: Section 2.6.7
$q_{z} := 0.00256 \cdot K_{z} \cdot K_{zt} \cdot K_{s} \cdot K_{e} \cdot K_{d} \cdot V^{2} \cdot psf$	$q_z = 30.83 \cdot psf$	Velocity Pressure ANSI/TIA-222-H: Section 2.6.11.6
$q_{zi} := 0.00256 \cdot K_z \cdot K_{zl} \cdot K_s \cdot K_e \cdot K_d \cdot V_i^2 \cdot psf$	$q_{zi} = 4.31 \cdot psf$	Velocity Pressure ANSI/TIA-222-H: Section 2.6.11.6
$q_{Zm} := 0.00256 \cdot K_{Z} \cdot K_{S} \cdot K_{e} \cdot K_{e} \cdot K_{d} \cdot V_{m}^{2} \cdot psf$	$q_{zm} = 2.42 \cdot psf$	Velocity Pressure ANSI/TIA-222-H: Section 2.6.11.6
SITE INFORMATION; Seismic Lateral Design

ASCE 7 Hazards Report

AMERICAN SOCIETY OF CIVIL ENGINEERS Address: No Address at This Location

Standard:	ASCE/SEI 7-16
Risk Category:	Ш
Soil Class:	D - Default (see Section 11.4.3)

Elevation: 624.28 ft (NAVD 88) Latitude: 42.72684 Longitude: -87.784674



Seismic

Results:

Site Soil Class:

D - Default (see Section 11.4.3)

S _s :	0.084	S _{D1} :	0.082
S ₁ :	0.051	T _L :	12
F _a :	1.6	PGA :	0.041
F _v :	2.4	PGA _M :	0.065
S _{MS} :	0.134	F _{PGA} :	1.6
S _{M1} :	0.123	l _e :	1
S _{DS} :	0.089	C _v :	0.7
Seismic Design Category	В		

Date: 6/2/2022

Importance Factor (Earthquake)	l _e := 1.0	ANSI/TIA-222-H: Table 2-3
Site Class	D - Stiff Soil (Default)	ANSI/TIA-222-H: Table 2-10
Seismic Design Category	В	
MCE.R Ground Motion (period=0.2s)	S _S := 0.084	
MCE.R Ground Motion (period=1.0s)	S ₁ := 0.051	
Seismic Design Value at 0.2s	S _{DS} := 0.089	
Long-Period Site Coefficient, Fv	$F_{V} = 2.4$	ANSI/TIA-222-H, Table 2-12
Seismic Design Value at 1.0s	S _{D1} := 0.076	$S_{D1} = 0.076$
Long-period Transition Period (s)	T _L := 12	
Response Modification Coefficient	<u>R</u> := 2	ANSI/TIA-222-H, 16.7
$C_{\text{scalc}} \coloneqq \frac{\left(S_{\text{DS}} \cdot I_{e}\right)}{R}$	$C_{SCalc} = 0.04$	Seismic Response Coefficient ANSI/TIA-222-H: 2.7.7.1.1
$C_{smin1} := 0.044 \cdot S_{DS} \cdot I_{e}$	$C_{smin1} = 0$	
$C_{smin2} := 0.03$ $C_{smin3} := \left \frac{\left(0.8 \cdot S_1 \cdot I_e \right)}{R} \text{if} S_1 \ge 0.6 \right $	$C_{smin2} = 0.03$	
C _{scalc} otherwise	$C_{smin3} = 0.04$	
$\begin{split} C_{s} &:= max \Big(C_{scalc}, C_{smin1}, C_{smin2}, C_{smin3} \Big) \\ A_{s1} &:= & \left \begin{array}{c} 1 \text{if} z \geq h_{mid} \\ \hline \frac{\left(3 \cdot h_{mid} \right) - \left(2 \cdot z \right)}{h_{mid}} \text{otherwise} \end{array} \right. \end{split}$	$C_{S} = 0.04$ $A_{S1} = 1$	Amplification Factor ANSI/TIA-222-H: 2.7.8.1 and 16.7
$A_{s} := \begin{array}{l} A_{s1} & \text{if Structure} = 1 \\ A_{s1} & \text{if Structure} = 2 \\ A_{s1} & \text{if Structure} = 3 \\ 3 & \text{if Structure} = 4 \\ 3 & \text{if Structure} = 5 \end{array}$	$A_S = 3$	









Antenna Mounting Pipe		
$H_{pipe} := 12 \cdot f$	Pipe := 2.5	
$Wt_{p1} := Weight_{total}$	$Wt_{p1} = 69.6 \text{ lbf}$	Total Weight of Pipe
$F_{p1} := F_p$	$F_{p1} = 95.89 \text{ lbf}$	Wind Load
$F_{p1_linear} := F_{p_linear}$	$F_{p1_linear} = 8 \cdot plf$	Linear Wind Load on Pipe
$DL_{ice,p1} := DL_{ice}$	$DL_{ice,p1} = 104.18 \text{ lbf}$	Total Weight of Ice
$DL_{ice.p1_linear} := \frac{DL_{ice}}{H_{pipe}}$	$DL_{ice.p1_linear} = 8.68 \cdot plf$	Linear Ice Load on Pipe
F _{p1i} := F _{pi}	$F_{p1i} = 28.44 \text{ lbf}$	Wind Load with Ice
$F_{p1i_linear} := F_{pi_linear}$	$F_{p1i_linear} = 2 \cdot plf$	Linear Wind Load with Ice on Pipe
$F_{p1m} := F_{pm}$	$F_{p1m} = 7.54 \text{ lbf}$	Wind Load (maintenance)
$F_{p1m_linear} := F_{pm_linear}$	$F_{p1m_linear} = 1 \cdot plf$	Linear Wind Load (maintenance) on Pipe
$F_{Ehp1} := Weight_{total} \cdot A_s \cdot C_s$	$F_{Ehp1} = 9.29 lbf$	Total Lateral Earthquake Load
$F_{Ehp1_linear} := \frac{F_{Ehp1}}{H_{pipe}}$	$F_{Ehp1_linear} = 0.77 \cdot plf$	Linear Lateral Earthquake Load
$F_{Evp1} := 0.2 \cdot S_{DS} \cdot Weight_{total}$	$F_{Evp1} = 1.24 \text{ lbf}$	Total Vertical Earthquake Load
$F_{Evp1_linear} := \frac{F_{Evp1}}{H_{pipe}}$	$F_{Evp1_linear} = 0.1 \cdot plf$	Linear Vertical Earthquake Load

SBWM:		
HeightWidth/Diameterheight := 14inwidth := 11.4in	Depth/DiameterWeightdepth := 2.5inweight := 8.13plf	<u>Shape</u> ● Flat ○ Round
$F_{FM1_linear} := F_{F_linear}$	$F_{FM1_linear} = 32 \cdot plf$	Linear Wind Load on Front Face
$F_{SM1_linear} := F_{S_linear}$	$F_{SM1_linear} = 8 \cdot plf$	Linear Wind Load on Side Face
$DL_{ice.M1_linear} := \frac{DL_{ice}}{height}$	$DL_{ice.M1_linear} = 15.48 \cdot plf$	Linear Ice Load on Member
$F_{FiM1_linear} := F_{Fi_linear}$	$F_{FiM1_linear} = 7 \cdot plf$	Linear Wind Load with Ice on Front Face
F _{SiM1_linear} := F _{Si_linear}	$F_{SiM1_linear} = 3 \cdot plf$	Linear Wind Load with Ice on Side Face
F _{FmM1_linear} := F _{Fm_linear}	F _{FmM1_linear} = 2·plf	Linear Wind Load (maintenance) on Front Face
F _{SmM1_linear} := F _{Sm_linear}	$F_{SmM1_linear} = 1 \cdot plf$	Linear Wind Load (maintenance) on Side Face
$F_{FM1} := F_F$	$F_{FM1} = 36.9 \cdot Ibf$	Wind Load on Front Face
$F_{SM1} := F_S$	$F_{SM1} = 9.02 \cdot lbf$	Wind Load on Side Face
$F_{FiM1} := F_{Fi}$	$F_{FiM1} = 8.09 \cdot lbf$	Wind Load with Ice on Front Face
$F_{SiM1} := F_{Si}$	$F_{SiM1} = 3.21 \cdot lbf$	Wind Load with Ice on Side Face
$F_{FmM1} := F_{Fm}$	$F_{FmM1} = 2.9 lbf$	Wind Load (maintenance) on Front Face
$F_{SmM1} := F_{Sm}$	$F_{SmM1} = 0.74 lbf$	Wind Load (maintenance) on Side Face
$DL_{ice.M1} := DL_{ice}$	$DL_{ice.M1} = 18.06 \text{ lbf}$	Total Weight of Ice
$Wt_{M1} := Weight_{total}$	$Wt_{M1} = 9.48 \text{ lbf}$	Total Weight of member
$F_{EhM1} := Weight_{total} \cdot A_{s} \cdot C_{s}$	$F_{EhM1} = 1.27 lbf$	Total Lateral Earthquake Load
$F_{EhM1_linear} := rac{F_{EhM1}}{height}$	$F_{EhM1_linear} = 1.09 \cdot plf$	Linear Lateral Earthquake Load
$F_{EvM1} := 0.2 \cdot S_{DS} \cdot Weight_{total}$	$F_{EvM1} = 0.17 lbf$	Total Vertical Earthquake Load
$F_{EvM1_linear} \coloneqq \frac{F_{EvM1}}{height}$	$F_{EvM1_linear} = 0.14 \cdot plf$	Linear Vertical Earthquake Load

Antenna Mounting Pipe		
Hpiper:= 9.fl	Pipe := 2.0	
$Wt_{p2} := Weight_{total}$	$Wt_{p2} = 32.94 \text{ lbf}$	Total Weight of Pipe
$F_{p2} := F_p$	$F_{p2} = 59.43 lbf$	Wind Load
$F_{p2_linear} := F_{p_linear}$	$F_{p2_linear} = 7 \cdot plf$	Linear Wind Load on Pipe
$DL_{ice.p2} := DL_{ice}$	$DL_{ice,p2} = 69.39 lbf$	Total Weight of Ice
$DL_{ice,p2_linear} := \frac{DL_{ice}}{H_{pipe}}$	$DL_{ice.p2_linear} = 7.71 \cdot plf$	Linear Ice Load on Pipe
$F_{p2i} := F_{pi}$	$F_{p2i} = 18.12 lbf$	Wind Load with Ice
$F_{p2i_linear} := F_{pi_linear}$	$F_{p2i_linear} = 2 \cdot plf$	Linear Wind Load with Ice on Pipe
$F_{p2m} := F_{pm}$	$F_{p2m} = 4.67 \text{ lbf}$	Wind Load (maintenance)
$F_{p2m_linear} := F_{pm_linear}$	$F_{p2m_linear} = 1 \cdot plf$	Linear Wind Load (maintenance) on Pipe
$F_{Ehp2} := Weight_{total} \cdot A_s \cdot C_s$	$F_{Ehp2} = 4.4 lbf$	Total Lateral Earthquake Load
$F_{Ehp2_linear} \coloneqq \frac{F_{Ehp2}}{H_{pipe}}$	$F_{Ehp2_linear} = 0.49 \cdot plf$	Linear Lateral Earthquake Load
$F_{Evp2} := 0.2 \cdot S_{DS} \cdot Weight_{total}$	$F_{Evp2} = 0.59 lbf$	Total Vertical Earthquake Load
$F_{Evp2_linear} \coloneqq \frac{F_{Evp2}}{H_{pipe}}$	$F_{Evp2_linear} = 0.07 \cdot plf$	Linear Vertical Earthquake Load

Mounting Pipe		
Hpiper:= 11.5·fi	<u>Pipe. := 3.0</u>	
Wtp2,:= Weight _{total}	$Wt_{p2} = 87.17 \text{ lbf}$	Total Weight of Pipe
Fp2.:= Fp	$F_{p2} = 111.68 lbf$	Wind Load
Fp2_linear. := Fp_linear	$F_{p2_linear} = 10 \cdot plf$	Linear Wind Load on Pipe
DL_{ice} = DL_{ice}	$DL_{ice,p2} = 113.68$ lbf	Total Weight of Ice
DLice DLice Hpipe	$DL_{ice.p2_linear} = 9.89.plf$	Linear Ice Load on Pipe
Fp2i = Fpi	$F_{p2i} = 28.29 lbf$	Wind Load with Ice
Fp2i_linear := Fpi_linear	$F_{p2i_linear} = 2 \cdot plf$	Linear Wind Load with Ice on Pipe
Fp2m. := Fpm	$F_{p2m} = 8.78 \text{ lbf}$	Wind Load (maintenance)
Fp2m_linear. := Fpm_linear	$F_{p2m_linear} = 1 \cdot plf$	Linear Wind Load (maintenance) on Pipe
FEhp2,:= Weight _{total} ·A _s ·C _s	$F_{Ehp2} = 11.64 lbf$	Total Lateral Earthquake Load
Fendentinear := Fendentiation Fendentiatio Fendentiation F	$F_{Ehp2_linear} = 1.01 \cdot plf$	Linear Lateral Earthquake Load
F _{Exp2} := 0.2⋅S _{DS} ⋅Weight _{total}	$F_{Evp2} = 1.55 lbf$	Total Vertical Earthquake Load
$F_{\text{Exp2-linear}} := \frac{F_{\text{Evp2}}}{H_{\text{pipe}}}$	$F_{Evp2_linear} = 0.13 \cdot plf$	Linear Vertical Earthquake Load



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z X		Code Check (Env) No Calc > 1.0 .90-1.0 .7590 .5075
	NC	050
	Narc	
	NO C	
	10 -23 -23	
	Nº fritte	
	NO 33 . 72	
Member Code Checks Disp Envelope Only Solution	layed (Enveloped)	
Fullerton Engineering Cons.		SK - 2
AA	Mount Analysis (Sector Alpha)	June 2, 2022 at 8:37 AM
MWMKE00116B	Unity Bending	MWMKE00120 - Mount Analysis (S

	WA WARD AND AND AND AND AND AND AND AND AND AN	
Envelope Only Solution		SK - 3
	Mount Analysis (Sector Alpha)	Une 2, 2022 at 0.22 AM
	Members	Page 21 of 108 Page 3





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Company Designer Job Number Model Name

: Fullerton Engineering Consultants, LLC

AA 1

MWMKE00116B Mount Analysis (Sector Alpha)

(Global) Model Settings

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation?	Yes
Increase Nailing Capacity for Wind?	Yes
Include Warping?	Yes
Trans Load Btwn Intersecting Wood Wall?	Yes
Area Load Mesh (in^2)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Include P-Delta for Walls?	Yes
Automatically Iterate Stiffness for Walls?	Yes
Max Iterations for Wall Stiffness	3
Gravity Acceleration (in/sec^2)	386.4
Wall Mesh Size (in)	12
Eigensolution Convergence Tol. (1.E-)	4
Vertical Axis	Υ
Global Member Orientation Plane	XZ
Static Solver	Sparse Accelerated
Dynamic Solver	Accelerated Solver
Hot Rolled Steel Code	AISC 15th(360-16): LRFD
Adjust Stiffness?	Yes(Iterative)
RISAConnection Code	AISC 15th(360-16): LRFD
Cold Formed Steel Code	AISI S100-16: LRFD
Wood Code	None
Wood Temperature	< 100F
Concrete Code	None
Masonry Code	None
Aluminum Code	None - Building
Stainless Steel Code	None

June 2, 2022 8:43 AM Checked By: BK



(Global) Model Settings, Continued

Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	Exact Integration
Parme Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections?	Yes
Use Cracked Sections Slab?	No
Bad Framing Warnings?	No
Unused Force Warnings?	Yes
Min 1 Bar Diam. Spacing?	No
Concrete Rebar Set	REBAR_SET_ASTMA615
Min % Steel for Column	1
Max % Steel for Column	8

Seismic Code	ASCE 7-16
Seismic Base Elevation (in)	Not Entered
Add Base Weight?	Yes
Ct X	.02
Ct Z	.02
T X (sec)	Not Entered
T Z (sec)	Not Entered
RX	3
RZ	3
Ct Exp. X	.75
Ct Exp. Z	.75
SD1	1
SDS	1
S1	1
TL (sec)	5
Risk Cat	l or ll
Drift Cat	Other
Om Z	1
Om X	1
Cd Z	1
Cd X	1
Rho Z	1
Rho X	1

Hot Rolled Steel Design Parameters

	Label	Shape	Length[in]	Lbyy[in]	Lbzz[in]	Lcomp top[in]	Lcomp bot[in]	L-torg	Kyy	Kzz	Cb	Function
1	M1	L3X3X4	14.5	12	12	12	12	12	2.1	2.1		Lateral
2	M2	L3X3X4	14.5	12	12	12	12	12	2.1	2.1		Lateral
3	M3	PIPE 2.5	144	48	48	48	48	48	2.1	2.1		Lateral
4	M14	SBWM	10.5			Lbyy			.65	.65		Lateral
5	M15	SBWM	10.5			Lbyy			.65	.65		Lateral

Material Takeoff

	Material	Size	Pieces	Length[in]	Weight[LB]
1	General				
2	RIGID		12	40	0
3	Total General		12	40	0
4					
5	Hot Rolled Steel				
6	A36 Gr.36	L3X3X4	2	29	11.842
7	A36 Gr.36	SBWM	2	21	17.936

[P:\...\...\...\...\...\...\MWMKE00120 - Mount Analysis (Sector Alpha & Gamma age 15 Page 33 of 108 RISA-3D Version 17.0.4



: Mount Analysis (Sector Alpha)

Material Takeoff (Continued)

	Material	Size	Pieces	Length[in]	Weight[LB]
8	A53 Gr. B	PIPE 2.5	1	144	65.742
9	Total HR Steel		5	194	95.519

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut	Area(Me	.Surface(
1	DL	None		-1		8				
2	DLi	None				8		3		
3	WL(0)	None				8		1		
4	WL(90)	None				8		3		
5	WL.i(0)	None				8		1		
6	WL.i(90)	None				8		3		
7	T	None								
8	EH(0)	None				8		3		
9	EH(90)	None				8		3		
10	EV	None				8		3		
11	WM(0)	None								
12	WM(90)	None								

Load Combinations

	Description	So	P	S	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac.	BLC	Fac	.BLC	Fac	.BLC	Fac.
1	1.4*DL	Yes	Υ		1	1.4																		
2	1.2*DL + 1.0* WL(0)) Yes	Υ		1	1.2	3	1																
3	1.2*DL + 1.0* WL(3.	Yes	Υ		1	1.2	3	.869	4	.5														
4	1.2*DL + 1.0* WL(6.	Yes	Υ		1	1.2	3	.5	4	.869														
5	1.2*DL + 1.0*WL(90)Yes	Υ		1	1.2	4	1																
6	1.2*DL + 1.0*WL(1	Yes	Υ		1	1.2	3	5	4	.869														
7	1.2*DL +1.0*WL(15.	Yes	Υ		1	1.2	3	869	4	.5														
8	1.2*DL + 1.0 * WL(. Yes	Υ		1	1.2	3	-1																
9	1.2*DL + 1.0* WL(2.	Yes	Υ		1	1.2	3	869	4	5														
10	1.2*DL + 1.0* WL(2.	Yes	Υ		1	1.2	3	5	4	869														
11	1.2*DL + 1.0*WL(2	Yes	Υ		1	1.2	4	-1																
12	1.2*DL + 1.0*WL(3	. Yes	Υ		1	1.2	3	.5	4	869														
13	1.2*DL +1.0*WL(33.	Yes	Υ		1	1.2	3	.869	4	5														
14	1.2*DL+1.0*DLi+1	. Yes	Υ		1	1.2	2	1	5	1	7	1												
15	1.2*DL+1.0*DLi+1	. Yes	Υ		1	1.2	2	1	5	.866	6	.5	7	1										
16	1.2*DL+1.0*DLi+1	.Yes	Υ		1	1.2	2	1	5	.5	6	.866	7	1										
17	1.2*DL+1.0*DLi+1	.Yes	Υ		1	1.2	2	1	6	1	7	1												
18	1.2*DL+1.0*DLi+1	.Yes	Υ		1	1.2	2	1	5	5	6	.866	7	1										
19	1.2*DL+1.0*DLi+1	.Yes	Υ		1	1.2	2	1	5	866	6	.5	7	1										
20	1.2*DL+1.0*DLi+1	.Yes	Υ		1	1.2	2	1	5	-1	7	1												
21	1.2*DL+1.0*DLi+1	.Yes	Υ		1	1.2	2	1	5	866	6	5	7	1										
22	1.2*DL+1.0*DLi+1	.Yes	Υ		1	1.2	2	1	5	5	6	866	7	1										
23	1.2*DL+1.0*DLi+1	.Yes	Υ		1	1.2	2	1	6	-1	7	1												
24	1.2*DL+1.0*DLi+1	.Yes	Υ		1	1.2	2	1	5	.5	6	866	7	1										
25	1.2*DL+1.0*DLi+1	.Yes	Υ		1	1.2	2	1	5	.866	6	5	7	1										
26	1.2*DL+1.0*EH(0)+.	.Yes	Υ		1	1.2	8	1	10	1														
27	1.2*DL+1.0*EH(0)+.	.Yes	Υ		1	1.2	8	1	10	-1														
28	1.2*DL+1.0*EH(90).	.Yes	Y		1	1.2	9	1	10	1														
29	1.2*DL+1.0*EH(90).	.Yes	Y		1	1.2	9	1	10	-1														
30	1.2*DL+1.0*EH(18	. Yes	Y		1	1.2	8	-1	10	1														
31	1.2*DL+1.0*EH(18	. Yes	Υ		1	1.2	8	-1	10	-1														
32	1.2*DL+1.0*EH(27	. Yes	Υ		1	1.2	9	-1	10	1														
33	1.2*DL+1.0*EH(27	. Yes	Y		1	1.2	9	-1	10	-1														
34	0.9*DL+1.0*EH(0)	Yes	Y		1	.9	8	1	10	-1														



Load Combinations (Continued)

	Description	SoP	. S	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac
35	0.9*DL+1.0*EH(0)	.Yes Y		1	.9	8	1	10	1														
36	0.9*DL+1.0*EH(90).	.Yes Y		1	.9	9	1	10	-1														
37	0.9*DL+1.0*EH(90).	.Yes Y		1	.9	9	1	10	1														
38	0.9*DL+1.0*EH(18	. Yes Y		1	.9	8	-1	10	-1														
39	0.9*DL+1.0*EH(18	.Yes Y		1	.9	8	-1	10	1														
40	0.9*DL+1.0*EH(27	. Yes Y		1	.9	9	-1	10	-1														
41	0.9*DL+1.0*EH(27	.Yes Y		1	.9	9	-1	10	1														
42	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	11	1														
43	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	11	.866	12	.5												
44	1.2*DL+1.5*LM1+1.	Yes Y		1	1.2	13	1.5	11	.5	12	.866												
45	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	12	1														
46	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	11	5	12	.866												
47	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	11	866	12	.5												
48	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	11	-1														
49	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	11	866	12	5												
50	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	11	5	12	866												
51	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	12	-1														
52	1.2*DL+1.5*LM1+1.	Yes Y		1	1.2	13	1.5	11	.5	12	866												
53	1.2*DL+1.5*LM1+1.	Yes Y		1	1.2	13	1.5	11	.866	12	5												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [lb-in]	LC	MY [lb-in]	LC	MZ [lb-in]	LC
1	N28	max	234.481	5	930.532	4	681.405	3	Ö	53	Ö	53	0 0	53
2		min	-234.961	11	-696.816	10	-783.269	9	0	1	0	1	0	1
3	N27	max	234.481	5	934.716	12	682.422	13	0	53	0	53	0	53
4		min	-234.961	11	-692.632	6	-782.25	7	0	1	0	1	0	1
5	N21	max	53.144	11	507.455	9	336.424	9	0	53	0	53	0	53
6		min	-52.664	5	-320.423	3	-234.439	3	0	1	0	1	0	1
7	N20	max	53.144	11	506.583	7	335.406	7	0	53	0	53	0	53
8		min	-52.664	5	-321.295	13	-235.457	13	0	1	0	1	0	1
9	Totals:	max	363.633	5	824.362	14	601.301	2						
10		min	-363.633	11	311.216	38	-601.301	8						

Envelope AISC 15th(360-16): LRFD Steel Code Checks

	Member	Shape	Coo	de Che	ck	Loc[in]	LC	SI	hear Ch	Loc[in] Dir	LC	phi*Pnc	.phi*Pnt [.	phi*Mn	phi*Mn	Cb	Eqn
1	M3	PIPE 2.5		.561		60	2		.045	58.5		8	28468.4	50715	43155	43155	1	H1-1b
2	M15	SBWM		.432		0	13		.150	4.266	Z	12	82203.8	97588.8	31644.4	356724	1.526	H1-1b
3	M14	SBWM		.334		0	8		.060	4.922	z	9	82203.8	97588.8	31644.4	356724	1.495	H1-1b
4	M2	L3X3X4		.235		7.25	10		.064	1.359	V	12	42313.8	46656	20257.6	.45068.9	1	H2-1
5	M1	L3X3X4		.115		7.25	9		.035	13.1	ý	9	42313.8	46656	20257.6	.45068.9	1	H2-1
		·							<u>ل</u>					•				



Wall Mount Connection Calculations (Sector Alpha)

New wall mounts will be attached to existing elevated roof wall via Thru-Bolts 1/2"Ø

Maximum Reactions from Risa Mount Analysis per one thru-bolt:

😳 Envel	ope Joint React	ions												
	Joint		X [lb]	L	Y [lb]	L	Z [lb]	L	MX [lb-i	Ĺ	MY [lb-i	L	MZ [lb-i	L
1	N28	max	234.481	5	930.532	4	681.405	3	0	53	0	53	0	53
2		min	-234.961	11	-696.816	10	-783.269	9	0	1	0	1	0	1
3	N27	max	234.481	5	934.716	12	682.422	13	0	53	0	53	0	53
4		min	-234.961	11	-692.632	6	-782.25	7	0	1	0	1	0	1
5	N20	max	53.144	11	506.583	7	335.406	7	0	53	0	53	0	53
6		min	-52.664	5	-321.295	13	-235.457	13	0	1	0	1	0	1
7	N21	max	53,144	11	507.455	9	336.424	9	0	53	0	53	0	53
8		min	-52.664	5	-320.423	3	-234.439	3	0	1	0	1	0	1
9	Totals:	max	363.633	5	824.362	14	601.301	2						
10		min	-363.633	11	311.216	38	-601.301	8						1

X := 234.961 lbf

Y := 930.532 lbf

Z := 783.269 lbf

$$\begin{split} \mathsf{P}_t &:= \mathsf{Z} \\ \mathsf{P}_v &:= \sqrt{\mathsf{X}^2 + \mathsf{Y}^2} \end{split}$$

d_b := 0.5in

 $A_b := 0.25 \pi \cdot {d_b}^2$

 $P_{t_bolt} := P_t$

 $P_{v \text{ bolt}} := P_{v}$

Maximum Factored Reaction - X direction Maximum Factored Reaction - Y direction Maximum Factored Reaction - Z direction

$P_t = 783.27 \text{ lbf}$	Factored Tensile Force
$P_{V} = 959.74 \text{ lbf}$	Factored Shear Force
	Diameter of thru-bolt
$A_b = 0.2 \cdot in^2$	Area of thru-bolt
$P_{t_bolt} = 783.27 \text{ lbf}$	Tension at each thru-bolt
$P_{v_bolt} = 959.74 \text{ lbf}$	Shear at each thru-bolt









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Company Designer Job Number Model Name

: Fullerton Engineering Consultants, LLC

AA 1

MWMKE00116B Mount Analysis (Sector Beta)

(Global) Model Settings

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation?	Yes
Increase Nailing Capacity for Wind?	Yes
Include Warping?	Yes
Trans Load Btwn Intersecting Wood Wall?	Yes
Area Load Mesh (in^2)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Include P-Delta for Walls?	Yes
Automatically Iterate Stiffness for Walls?	Yes
Max Iterations for Wall Stiffness	3
Gravity Acceleration (in/sec^2)	386.4
Wall Mesh Size (in)	12
Eigensolution Convergence Tol. (1.E-)	4
Vertical Axis	Y
Global Member Orientation Plane	XZ
Static Solver	Sparse Accelerated
Dynamic Solver	Accelerated Solver
Hot Rolled Steel Code	AISC 15th(360-16): LRFD
Adjust Stiffness?	Yes(Iterative)
RISAConnection Code	AISC 15th(360-16): LRFD
Cold Formed Steel Code	AISI S100-16: LRFD
Wood Code	None
Wood Temperature	< 100F
Concrete Code	None
Masonry Code	None
Aluminum Code	None - Building
Stainless Steel Code	None

June 2, 2022 10:30 AM Checked By: BK



(Global) Model Settings, Continued

Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	Exact Integration
Parme Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections?	Yes
Use Cracked Sections Slab?	No
Bad Framing Warnings?	No
Unused Force Warnings?	Yes
Min 1 Bar Diam. Spacing?	No
Concrete Rebar Set	REBAR_SET_ASTMA615
Min % Steel for Column	1
Max % Steel for Column	8

Seismic Code	ASCE 7-16
Seismic Base Elevation (in)	Not Entered
Add Base Weight?	Yes
Ct X	.02
Ct Z	.02
T X (sec)	Not Entered
T Z (sec)	Not Entered
RX	3
RZ	3
Ct Exp. X	.75
Ct Exp. Z	.75
SD1	1
SDS	1
S1	1
TL (sec)	5
Risk Cat	l or ll
Drift Cat	Other
Om Z	1
Om X	1
Cd Z	1
Cd X	1
Rho Z	1
Rho X	1

Hot Rolled Steel Design Parameters

	Label	Shape	Length[in]	Lbyy[in]	Lbzz[in]	Lcomp top[in]	Lcomp bot[in]	L-torg	Kyy	Kzz	Cb	Function
1	M1	L3X3X4	20	12	12	12	12	12	2.1	2.1		Lateral
2	M2	L3X3X4	20	12	12	12	12	12	2.1	2.1		Lateral
3	M3	Pipe 2.0	132	48	48	48	48	48	2.1	2.1		Lateral

Material Takeoff

	Material	Size	Pieces	Length[in]	Weight[LB]
1	General			•••	
2	RIGID		4	10	0
3	Total General		4	10	0
4					
5	Hot Rolled Steel				
6	A36 Gr.36	L3X3X4	2	40	16.333
7	A53 Gr. B	Pipe 2.0	1	132	38.179
8	Total HR Steel		3	172	54.513



Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut	.Area(Me	Surface(
1	DL	None		-1		2			,	,
2	DLi	None				2		1		
3	WL(0)	None				2		1		
4	WL(90)	None				2		1		
5	WL.i(0)	None				2		1		
6	WL.i(90)	None				2		1		
7	T	None								
8	EH(0)	None				2		1		
9	EH(90)	None				2		1		
10	EV	None				2		1		
11	WM(0)	None								
12	WM(90)	None								

Load Combinations

	Description	SoI	P	S	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac
1	1.4*DL	Yes	Υ		1	1.4																		
2 1.2*0	DL + 1.0* WL(0)	Yes	Υ		1	1.2	3	1																
3 1.2*0	DL + 1.0* WL(3	Yes	Υ		1	1.2	3	.869	4	.5														
4 1.2*0	DL + 1.0* WL(6	Yes	Y		1	1.2	3	.5	4	.869														
5 1.2*C	DL + 1.0*WL(90)	Yes	Υ		1	1.2	4	1																
6 1.2*0	DL + 1.0*WL(1	Yes	Υ		1	1.2	3	5	4	.869														
7 1.2*0	DL +1.0*WL(15	Yes	Υ		1	1.2	3	869	4	.5														
8 1.2*0	DL + 1.0 * WL(Yes	Υ		1	1.2	3	-1																
9 1.2*0	DL + 1.0* WL(2	Yes	Υ		1	1.2	3	869	4	5														
10 1.2*0	DL + 1.0* WL(2	Yes	Y		1	1.2	3	5	4	869														
11 1.2*	DL + 1.0*WL(2	Yes	Υ		1	1.2	4	-1																
12 1.2*	DL + 1.0*WL(3	Yes	Y		1	1.2	3	.5	4	869														
13 1.2*	DL +1.0*WL(33	Yes	Υ		1	1.2	3	.869	4	5														
14 1.2*	DL+1.0*DLi+1	Yes	Y		1	1.2	2	1	5	1	7	1												
15 1.2*	DL+1.0*DLi+1	Yes	Υ		1	1.2	2	1	5	.866	6	.5	7	1										
16 1.2*	DL+1.0*DLi+1	Yes	Y		1	1.2	2	1	5	.5	6	.866	7	1										
17 1.2*0	DL+1.0*DLi+1	Yes	Υ		1	1.2	2	1	6	1	7	1												
18 1.2*0	DL+1.0*DLi+1	Yes	Y		1	1.2	2	1	5	5	6	.866	7	1										
19 1.2*0	DL+1.0*DLi+1	Yes	Υ		1	1.2	2	1	5	866	6	.5	7	1										
20 1.2*	DL+1.0*DLi+1	Yes	Y		1	1.2	2	1	5	-1	7	1												
21 1.2*	DL+1.0*DLi+1	Yes	Υ		1	1.2	2	1	5	866	6	5	7	1										
22 1.2*E	DL+1.0*DLi+1	Yes	Υ		1	1.2	2	1	5	5	6	866	7	1										
23 1.2*	DL+1.0*DLi+1	Yes	Υ		1	1.2	2	1	6	-1	7	1												
24 1.2*0	DL+1.0*DLi+1	Yes	Y		1	1.2	2	1	5	.5	6	866	7	1										
25 1.2*	DL+1.0*DLi+1	Yes	Υ		1	1.2	2	1	5	.866	6	5	7	1										
26 1.2*	DL+1.0*EH(0)+	Yes	Y		1	1.2	8	1	10	1														
27 1.2*0	DL+1.0*EH(0)+	Yes	Υ		1	1.2	8	1	10	-1														
28 1.2*	DL+1.0*EH(90)	Yes	Y		1	1.2	9	1	10	1														
<u>29</u> 1.2*E	DL+1.0*EH(90)	Yes	Υ		1	1.2	9	1	10	-1														
30 1.2*	DL+1.0*EH(18	Yes	Y		1	1.2	8	-1	10	1														
31 1.2*	DL+1.0*EH(18	Yes	Υ		1	1.2	8	-1	10	-1														
<u>32</u> 1.2*E	DL+1.0*EH(27	Yes	Y		1	1.2	9	-1	10	1														
33 1.2*0	DL+1.0*EH(27	Yes	Υ		1	1.2	9	-1	10	-1														
34 0.9*E	DL+1.0*EH(0)	Yes	Y		1	.9	8	1	10	-1														
35 0.9*	DL+1.0*EH(0)	Yes	Y		1	.9	8	1	10	1														
36 0.9*	DL+1.0*EH(90)	Yes	Y		1	.9	9	1	10	-1														
37 0.9*	DL+1.0*EH(90)	Yes	Y		1	.9	9	1	10	1														
38 0.9*	DL+1.0*EH(18	Yes	Y		1	.9	8	-1	10	-1														
39 0.9*E	DL+1.0*EH(18	Yes	Y		1	.9	8	-1	10	1														



Load Combinations (Continued)

	Description	So	P	S	BLC	Fac	BLC	Fac	.BLC	Fac	BLC	Fac	BLC	Fac	.BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac
40	0.9*DL+1.0*EH(27	Yes	Υ		1	.9	9	-1	10	-1														
41	0.9*DL+1.0*EH(27	Yes	Υ		1	.9	9	-1	10	1														
42	1.2*DL+1.5*LM1+1	Yes	Υ		1	1.2	13	1.5	11	1														
43	1.2*DL+1.5*LM1+1	Yes	Υ		1	1.2	13	1.5	11	.866	12	.5												
44	1.2*DL+1.5*LM1+1	Yes	Υ		1	1.2	13	1.5	11	.5	12	.866												
45	1.2*DL+1.5*LM1+1	Yes	Υ		1	1.2	13	1.5	12	1														
46	1.2*DL+1.5*LM1+1	Yes	Υ		1	1.2	13	1.5	11	5	12	.866												
47	1.2*DL+1.5*LM1+1	Yes	Υ		1	1.2	13	1.5	11	866	12	.5												
48	1.2*DL+1.5*LM1+1	Yes	Υ		1	1.2	13	1.5	11	-1														
49	1.2*DL+1.5*LM1+1	Yes	Y		1	1.2	13	1.5	11	866	12	5												
50	1.2*DL+1.5*LM1+1	Yes	Υ		1	1.2	13	1.5	11	5	12	866												
51	1.2*DL+1.5*LM1+1	Yes	Υ		1	1.2	13	1.5	12	-1														
52	1.2*DL+1.5*LM1+1	Yes	Y		1	1.2	13	1.5	11	.5	12	866												
53	1.2*DL+1.5*LM1+1	Yes	Y		1	1.2	13	1.5	11	.866	12	5												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [lb-in]	LC	MY [lb-in]	LC	MZ [lb-in]	LC
1	N20	max	.437	17	893.01	8	162.534	8	Ö	53	Ö	53	0 0	53
2		min	437	23	-767.5	2	-147.418	2	0	1	0	1	0	1
3	N21	max	.437	17	893.01	8	162.534	8	0	53	0	53	0	53
4		min	437	23	-767.5	2	-147.418	2	0	1	0	1	0	1
5	N27	max	124.15	5	942.076	13	361.653	2	0	53	0	53	0	53
6		min	-124.15	11	-885.639	7	-376.768	8	0	1	0	1	0	1
7	N28	max	124.15	5	942.076	3	361.653	2	0	53	0	53	0	53
8		min	-124.15	11	-885.639	9	-376.768	8	0	1	0	1	0	1
9	Totals:	max	247.535	5	414.035	14	428.47	2						
10		min	-247.535	11	134.511	38	-428.469	8						

Envelope AISC 15th(360-16): LRFD Steel Code Checks

	Member	Shape	Code Check	Loc[in]	LC	Shear Ch.	Loc[in]	Dir LC	phi*Pnc.	phi*Pnt [.	phi*Mn	phi*Mn	Cb	Eqn
1	M3	Pipe 2.0	.649	59.1	8	.049	59.1	13	13787.8	32130	22459.5	22459.5	1	H1-1b
2	M1	L3X3X4	.367	10	8	.061	1.25	y 8	42313.8	46656	20257.6	.45068.9	1	H2-1
3	M2	L3X3X4	.360	10	13	.065	1.25	y 13	42313.8	46656	20257.6.	.45068.9	1	H2-1
			Max. S Memb	Stress ers ar	Ra re a	tio<1 dequate	•							

Wall Mount Connection Calculations (Sector Beta)

New wall mounts will be attached to existing stairwell wall via Thru-Bolts 1/2"Ø

Maximum Reactions from Risa Mount Analysis per one thru-bolt:

Envel	ope Joint React	ions												-Σ
	Joint		X [lb]	L	Y [lb]	L	Z [lb]	L	MX [lb-i	L	MY [lb-i	L	MZ [Ib-i	L
1	N27	max	124.15	5	942.076	13	361.653	2	0	53	0	53	0	53
2		min	-124.15	11	-885.639	7	-376.768	8	0	1	0	1	0	1
3	N28	max	124.15	5	942.076	3	361.653	2	0	53	0	53	0	53
4		min	-124.15	11	-885.639	9	-376.768	8	0	1	0	1	0	1
5	N20	max	.437	17	893.01	8	162.534	8	0	53	0	53	0	53
6		min	437	23	-767.5	2	-147.418	2	0	1	0	1	0	1
7	N21	max	.437	17	893.01	8	162.534	8	0	53	0	53	0	53
8		min	437	23	-7 <mark>67</mark> .5	2	-147.418	2	0	1	0	-	0	1
9	Totals:	max	247.535	5	414.035	14	428.47	2						
10		min	-247.535	11	134.511	38	-428.469	8						

X := 124.15lbf

Y:= 942.076lbf

<u>Z</u> := 376.768lbf

 $\begin{array}{l} \underset{\text{Pt}}{\text{Pt}} \coloneqq \text{Z} \\ \underset{\text{Pt}}{\text{Pt}} \coloneqq \sqrt{\text{X}^2 + \text{Y}^2} \end{array}$

db := 0.5in

 $\underline{A}_{b} := 0.25 \pi \cdot {d_b}^2$

Pt.bolt := Pt

Publit := Pv

Maximum Factored Reaction - X direction Maximum Factored Reaction - Y direction Maximum Factored Reaction - Z direction

$P_t = 376.77 \text{lbf}$	Factored Tensile Force
$P_V = 950.22 \text{ lbf}$	Factored Shear Force
	Diameter of thru-bolt
$A_b = 0.2 \cdot in^2$	Area of thru-bolt
$P_{t_bolt} = 376.77 \text{ lbf}$	Tension at each thru-bolt
$P_{v, \text{bolt}} = 950.22 \text{lbf}$	Shear at each thru-bolt





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z X	WE W	Code Check (Env) - No Calc -> 10 - 75-90 -50-75 050
Member Code Checks Displaye Envelope Only Solution	d (Enveloped)	
Fullerton Engineering Cons.		SK - 2
AA	Mount Analysis (Sector Gamma)	June 2, 2022 at 9·21 AM
	wount Analysis (Sector Gamma)	
MWMKE00116B	Unity Bending	MWMKE00120 - Mount Analysis (S

z X		
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	1115M136	
	AN14M12	
	fann Mar	
Envelope Only Solution		
Fullerton Engineering Cons		SK - 3
AA	Mount Analysis (Sector Gamma)	June 2, 2022 at 9:22 AM
MWMKE00116B	Members	MWMKE00120 - Mount Analysis (S
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Company Designer Job Number Model Name

: Fullerton Engineering Consultants, LLC

AA 1

MWMKE00116B Mount Analysis (Sector Gamma)

(Global) Model Settings

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation?	Yes
Increase Nailing Capacity for Wind?	Yes
Include Warping?	Yes
Trans Load Btwn Intersecting Wood Wall?	Yes
Area Load Mesh (in^2)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Include P-Delta for Walls?	Yes
Automatically Iterate Stiffness for Walls?	Yes
Max Iterations for Wall Stiffness	3
Gravity Acceleration (in/sec^2)	386.4
Wall Mesh Size (in)	12
Eigensolution Convergence Tol. (1.E-)	4
Vertical Axis	Y
Global Member Orientation Plane	XZ
Static Solver	Sparse Accelerated
Dynamic Solver	Accelerated Solver
Hot Rolled Steel Code	AISC 15th(360-16): LRFD
Adjust Stiffness?	Yes(Iterative)
RISAConnection Code	AISC 15th(360-16): LRFD
Cold Formed Steel Code	AISI S100-16: LRFD
Wood Code	None
Wood Temperature	< 100F
Concrete Code	None
Masonry Code	None
Aluminum Code	None - Building
Stainless Steel Code	None

June 2, 2022 10:04 AM Checked By: BK



(Global) Model Settings, Continued

Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	Exact Integration
Parme Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections?	Yes
Use Cracked Sections Slab?	No
Bad Framing Warnings?	No
Unused Force Warnings?	Yes
Min 1 Bar Diam. Spacing?	No
Concrete Rebar Set	REBAR_SET_ASTMA615
Min % Steel for Column	1
Max % Steel for Column	8

Seismic Code	ASCE 7-16
Seismic Base Elevation (in)	Not Entered
Add Base Weight?	Yes
Ct X	.02
Ct Z	.02
T X (sec)	Not Entered
T Z (sec)	Not Entered
RX	3
RZ	3
Ct Exp. X	.75
Ct Exp. Z	.75
SD1	1
SDS	1
S1	1
TL (sec)	5
Risk Cat	l or ll
Drift Cat	Other
Om Z	1
Om X	1
Cd Z	1
Cd X	1
Rho Z	1
Rho X	1

Hot Rolled Steel Design Parameters

	Label	Shape	Length[in]	Lbyy[in]	Lbzz[in]	Lcomp top[in]	Lcomp bot[in]	L-torg	Kyy	Kzz	Cb	Function
1	M1	L3X3X4	14.5	12	12	12	12	12	2.1	2.1		Lateral
2	M2	L3X3X4	14.5	12	12	12	12	12	2.1	2.1		Lateral
3	M3	PIPE 2.5	144	48	48	48	48	48	2.1	2.1		Lateral
4	M14	SBWM	10.5			Lbvy			.65	.65		Lateral
5	M15	SBWM	10.5			Lbyy			.65	.65		Lateral

Material Takeoff

	Material	Size	Pieces	Length[in]	Weight[LB]
1	General				
2	RIGID		12	40	0
3	Total General		12	40	0
4					
5	Hot Rolled Steel				
6	A36 Gr.36	L3X3X4	2	29	11.842
7	A36 Gr.36	SBWM	2	21	17.936

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Material Takeoff (Continued)

	Material	Size	Pieces	Length[in]	Weight[LB]
8	A53 Gr. B	PIPE 2.5	1	144	65.742
9	Total HR Steel	_	5	194	95.519

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut	Area(Me	.Surface(
1	DL	None		-1		8				
2	DLi	None				8		3		
3	WL(0)	None				8		1		
4	WL(90)	None				8		3		
5	WL.i(0)	None				8		1		
6	WL.i(90)	None				8		3		
7	T	None								
8	EH(0)	None				8		3		
9	EH(90)	None				8		3		
10	EV	None				8		3		
11	WM(0)	None								
12	WM(90)	None								

Load Combinations

	Description	SoP.	. S.	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	.BLC	Fac	BLC	Fac	.BLC	Fac
1	1.4*DL	Yes Y	1	1	1.4																		
2	1.2*DL + 1.0* WL(0) Yes Y	1	1	1.2	3	1																
3	1.2*DL + 1.0* WL(3	Yes	'	1	1.2	3	.869	4	.5														
4	1.2*DL + 1.0* WL(6	Yes Y	1	1	1.2	3	.5	4	.869														
5	1.2*DL + 1.0*WL(90)Yes	1	1	1.2	4	1																
6	1.2*DL + 1.0*WL(1.	Yes	1	1	1.2	3	5	4	.869														
7	1.2*DL +1.0*WL(15	Yes	'	1	1.2	3	869	4	.5														
8	1.2*DL + 1.0 * WL(.	Yes Y	1	1	1.2	3	-1																
9	1.2*DL + 1.0* WL(2	Yes	'	1	1.2	3	869	4	5														
10	1.2*DL + 1.0* WL(2	Yes Y	1	1	1.2	3	5	4	869														
11	1.2*DL + 1.0*WL(2.	Yes	1	1	1.2	4	-1																
12	1.2*DL + 1.0*WL(3.	Yes Y	1	1	1.2	3	.5	4	869														
13	1.2*DL +1.0*WL(33	Yes	'	1	1.2	3	.869	4	5														
14	1.2*DL+1.0*DLi+1	Yes γ	1	1	1.2	2	1	5	1	7	1												
15	1.2*DL+1.0*DLi+1	Yes γ	1	1	1.2	2	1	5	.866	6	.5	7	1										
16	1.2*DL+1.0*DLi+1	Yes γ	/	1	1.2	2	1	5	.5	6	.866	7	1										
17	1.2*DL+1.0*DLi+1	Yes Y	1	1	1.2	2	1	6	1	7	1												
18	1.2*DL+1.0*DLi+1	Yes γ	1	1	1.2	2	1	5	5	6	.866	7	1										
19	1.2*DL+1.0*DLi+1	Yes γ	1	1	1.2	2	1	5	866	6	.5	7	1										
20	1.2*DL+1.0*DLi+1	Yes γ	1	1	1.2	2	1	5	-1	7	1												
21	1.2*DL+1.0*DLi+1	Yes γ	/	1	1.2	2	1	5	866	6	5	7	1										
22	1.2*DL+1.0*DLi+1	Yes γ	1	1	1.2	2	1	5	5	6	866	7	1										
23	1.2*DL+1.0*DLi+1	Yes γ	1	1	1.2	2	1	6	-1	7	1												
24	1.2*DL+1.0*DLi+1	Yes γ	·	1	1.2	2	1	5	.5	6	866	7	1										
25	1.2*DL+1.0*DLi+1	Yes	·	1	1.2	2	1	5	.866	6	5	7	1										
26	1.2*DL+1.0*EH(0)+	Yes Ŋ	·	1	1.2	8	1	10	1														
27	1.2*DL+1.0*EH(0)+	Yes γ	·	1	1.2	8	1	10	-1														
28	1.2*DL+1.0*EH(90)	Yes	1	1	1.2	9	1	10	1														
29	1.2*DL+1.0*EH(90)	Yes Y	1	1	1.2	9	1	10	-1														
30	1.2*DL+1.0*EH(18	. Yes Y	1	1	1.2	8	-1	10	1														
31	1.2*DL+1.0*EH(18	. Yes Y	1	1	1.2	8	-1	10	-1														
32	1.2*DL+1.0*EH(27	Yes Y	1	1	1.2	9	-1	10	1														
33	1.2*DL+1.0*EH(27	Yes	1	1	1.2	9	-1	10	-1														
34	0.9*DL+1.0*EH(0)	Yes	1	1	.9	8	1	10	-1														

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Load Combinations (Continued)

	Description	SoP	S	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac	BLC	Fac
35	0.9*DL+1.0*EH(0)	.Yes Y		1	.9	8	1	10	1														
36	0.9*DL+1.0*EH(90).	.Yes Y		1	.9	9	1	10	-1														
37	0.9*DL+1.0*EH(90).	.Yes Y		1	.9	9	1	10	1														
38	0.9*DL+1.0*EH(18	. Yes Y		1	.9	8	-1	10	-1														
39	0.9*DL+1.0*EH(18	Yes Y		1	.9	8	-1	10	1														
40	0.9*DL+1.0*EH(27	. Yes Y		1	.9	9	-1	10	-1														
41	0.9*DL+1.0*EH(27	.Yes Y		1	.9	9	-1	10	1														
42	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	11	1														
43	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	11	.866	12	.5												
44	1.2*DL+1.5*LM1+1.	Yes Y		1	1.2	13	1.5	11	.5	12	.866												
45	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	12	1														
46	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	11	5	12	.866												
47	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	11	866	12	.5												
48	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	11	-1														
49	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	11	866	12	5												
50	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	11	5	12	866												
51	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	12	-1														
52	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	11	.5	12	866												
53	1.2*DL+1.5*LM1+1.	.Yes Y		1	1.2	13	1.5	11	.866	12	5												

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [lb-in]	LC	MY [lb-in]	LC	MZ [lb-in]	LC
1	N20	max	46.155	11	496.353	13	188.413	7	Ö	53	Ö	53	0	53
2		min	-45.676	5	-258.408	7	-325.429	13	0	1	0	1	0	1
3	N21	max	46.155	11	495.484	3	189.428	9	0	53	0	53	0	53
4		min	-45.676	5	-259.277	9	-324.414	3	0	1	0	1	0	1
5	N27	max	227.497	5	835.703	6	771.33	13	0	53	0	53	0	53
6		min	-227.976	11	-652.485	12	-634.437	7	0	1	0	1	0	1
7	N28	max	227.497	5	839.875	10	770.315	3	0	53	0	53	0	53
8		min	-227.976	11	-648.312	4	-635.451	9	0	1	0	1	0	1
9	Totals:	max	363.641	5	824.364	14	601.315	2						
10		min	-363.641	11	311.216	38	-601.319	8						

Envelope AISC 15th(360-16): LRFD Steel Code Checks

	Member	Shape	Code Ch	eck Loc[in]	LC	Shear Ch	Loc[in]	Dir	LC p	hi*Pnc	.phi*Pnt [.	phi*Mn	phi*Mn	Cb	Eqn
1	M3	PIPE 2.5	.516	60	2	.045	58.5		2 2	28468.4	50715	43155	43155	1	H1-1b
2	M15	SBWM	.384	0	9	.136	4.375	Ζ	108	32203.8	97588.8	31644.4	356724	1.531	H1-1b
3	M14	SBWM	.327	0	2	.058	5.031	z	138	32203.8	97588.8	31644.4	356724	1.495	H1-1b
4	M2	L3X3X4	.221	7.25	12	.058	13.1	V	104	2313.8	46656	20257.6	45068.9	1	H2-1
5	M1	L3X3X4	.113	7.25	13	.034	1.359	ý	134	2313.8	46656	20257.6	45068.9	1	H2-1



Wall Mount Connection Calculations (Sector Gamma)

New wall mounts will be attached to existing parapet wall via Thru-Bolts $\frac{1}{2}$ "Ø

Maximum Reactions from Risa Mount Analysis per one thru-bolt:

3 Envelope Joint Reactions											2			
	Joint		X [lb]	L	Y [lb]	L	Z [lb]	L	MX [lb-i	L	MY [lb-i	L	MZ [lb-i	L
1	N20	max	46.155	11	496.353	13	<mark>188.41</mark> 3	7	0	53	0	53	0	53
2		min	-45.676	5	-258.408	7	-325.429	13	0	1	0	1	0	1
3	N21	max	46.155	11	495.484	3	189.428	9	0	53	0	53	0	53
4		min	-45.676	5	-259.277	9	-324.414	3	0	1	0	1	0	1
5	N27	max	227.497	5	835.703	6	771.33	13	0	53	0	53	0	53
6		min	-227.976	11	-652.485	12	-634.437	7	0	1	0	-	0	1
7	N28	max	227.497	5	839.875	10	770.315	3	0	53	0	53	0	53
8		min	-227.976	11	-648.312	4	-635.451	9	0	1	0	1	0	1
9	Totals:	max	363.641	5	824.364	14	<mark>601.315</mark>	2						
10		min	-363.641	11	311.216	38	-601.319	8						

X,:= 227.976lbf	Maxim
Y. := 839.875lbf	Maxim
$Z_{\rm M} := 635.451 \text{lbf}$	Maxin
Pt:= Z	$P_t = d$
$P_{XX} := \sqrt{X^2 + Y^2}$	$P_V =$
d _b := 0.5in	
$A_{b} := 0.25\pi \cdot d_{b}^{2}$	$A_b =$
Pt_botty:= Pt	P _{t_bolt}

Publit := Pv

Maximum Factored Reaction - X direction Maximum Factored Reaction - Y direction Maximum Factored Reaction - Z direction

$P_t = 635.45 \text{lbf}$	Factored Tensile Force
$P_{V} = 870.27 \text{ lbf}$	Factored Shear Force
	Diameter of thru-bolt
$A_{b} = 0.2 \cdot in^{2}$	Area of thru-bolt
$P_{t_bolt} = 635.45 \text{ lbf}$	Tension at each thru-bolt
$P_{v \text{ bolt}} = 870.27 \text{ lbf}$	Shear at each thru-bolt

Tensile and Shear Strength of Thru-Bolts		
Fut := 45ksi		Nominal tensile strength per AISC 360, Table J3.2
F _{TW} := 27ksi		Nominal shear strength per AISC 360, Table J3.2
= 0.75		Resistance Factor (LRFD - AISC 360, Section J3-6)
$R_{\text{Rtt}} := \Phi_{\text{bolt}} \cdot F_{\text{nt}} \cdot A_{\text{b}}$	$R_{nt} = 6.63 \cdot kip$	Design Nominal Tensile Strength (AISC 360, Section J3-1)
$R_{RXA} := \Phi_{bolt} \cdot F_{nv} \cdot A_b$	$R_{nv} = 3.98 \cdot kip$	Design Nominal Shear Strength (AISC 360, Section J3-1)
$\frac{P_{t_bolt}}{R_{nt}} = 9.59.\%$	$\frac{P_{v_bolt}}{R_{nv}} = 21.89.\%$	
Check = "Thru-Bolts are adequate. Effects of combined stress	don't need to be investigated because rat	io of either tension or shear is under 30%"









C12x20.7:		
HeightWidth/Diameterheight := 36inwidth := 12in	Depth/DiameterWeightdepth := 2.94inweight := 20.7plf	<u>Shape</u> ● Flat ○ Round
FEMILINEAR = FF_linear	$F_{FM1_linear} = 34 \cdot plf$	Linear Wind Load on Front Face
FSM1_linear := FS_linear	$F_{SM1_linear} = 11 \cdot plf$	Linear Wind Load on Side Face
DLice Millinear := DLice height	$DL_{ice.M1_linear} = 13.05 \cdot plf$	Linear Ice Load on Member
Fillinear = Fri_linear	$F_{FiM1_linear} = 6 \cdot plf$	Linear Wind Load with Ice on Front Face
FsiMillingar := Fsi_linear	$F_{SiM1_linear} = 3 \cdot plf$	Linear Wind Load with Ice on Side Face
FEMIL:= FF	$F_{FM1} = 101.74 \cdot lbf$	Wind Load on Front Face
FSM1 = FS	$F_{SM1} = 32.12 \cdot lbf$	Wind Load on Side Face
FEIMIN:= F _{Fi}	$F_{FiM1} = 19.28 \cdot lbf$	Wind Load with Ice on Front Face
F _{SIMM} := F _{Si}	$F_{SiM1} = 8.87 \cdot lbf$	Wind Load with Ice on Side Face
DLice DLice	$DL_{ice.M1} = 39.16 lbf$	Total Weight of Ice
Wtww:= Weighttotal	$Wt_{M1} = 62.1 \text{ lbf}$	Total Weight of member
$F_{EhM1} := Weight_{total} \cdot A_s \cdot C_s$	$F_{EhM1} = 8.29 lbf$	Total Lateral Earthquake Load
$F_{EhM1} = \frac{F_{EhM1}}{height}$	$F_{EhM1_linear} = 2.76 \cdot plf$	Linear Lateral Earthquake Load
FEXML := 0.2.S _{DS} .Weight _{total}	$F_{EvM1} = 1.11 \text{ lbf}$	Total Vertical Earthquake Load
FEXMINIAR := FEVM1 height	$F_{EvM1_linear} = 0.37 \cdot plf$	Linear Vertical Earthquake Load




P1000 Unistrut:				
<u>Height</u> <u>Wid</u> height := 58in	Ith/DiameterDepthh. := 1.625indepth	∕ <mark>Diameter</mark> ≔ 1.625in	<u>Weight</u> weight := 1.52plf	<u>Shape</u> ● Flat ○ Round
Datu:				
FEMILINEAR = FF_linear		$F_{FM1_linear} = 8$	³ ·plf	Linear Wind Load on Front Face
FSMInlinear := FS_linear		$F_{SM1_linear} = 8$	3∙plf	Linear Wind Load on Side Face
$\frac{DL_{ice}}{height} := \frac{DL_{ice}}{height}$		DL _{ice.M1_linear}	= 9.59 · plf	Linear Ice Load on Member
Frimminger := Fri_linear		F _{FiM1_linear} = 3	3∙plf	Linear Wind Load with Ice on Front Face
Fsimillinear := Fsi_linear		F _{SiM1_linear} = 3	3·plf	Linear Wind Load with Ice on Side Face
FEMIN:= FF		$F_{FM1} = 36.32 \cdot I$	bf	Wind Load on Front Face
FSMI := FS		$F_{SM1} = 36.32 \cdot I$	bf	Wind Load on Side Face
FEININ:= F _{Fi}		$F_{FiM1} = 12.59$ ·	lbf	Wind Load with Ice on Front Face
F _{SIM1} := F _{Si}		$F_{SiM1} = 12.59$.	lbf	Wind Load with Ice on Side Face
DLice DLice		$DL_{ice.M1} = 46.3$	36 lbf	Total Weight of Ice
Wtwi.:= Weighttotal		$Wt_{M1} = 7.35 lb$	f	Total Weight of member
$F_{\text{EhM1}} := \text{Weight}_{\text{total}} \cdot A_s \cdot C_s$		$F_{EhM1} = 0.98 II$	bf	Total Lateral Earthquake Load
FEHMILLINGER := FEHMI height		F _{EhM1_linear} =	0.2•plf	Linear Lateral Earthquake Load
FEXML := 0.2.Sps.Weighttotal		$F_{EvM1} = 0.13 lk$	of	Total Vertical Earthquake Load
Fevminicar:= Fevmi height		F _{EvM1_linear} =	0.03•plf	Linear Vertical Earthquake Load

H-Frame Vertical Pipe		
H _{pipe} = 5.fl	Pipe := 3.0	
Wtp2 := Weight _{total}	$Wt_{p2} = 37.9 lbf$	Total Weight of Pipe
Fp2. = Fp	$F_{p2} = 41.49 lbf$	Wind Load
Fp2_linear := Fp_linear	$F_{p2_linear} = 8 \cdot plf$	Linear Wind Load on Pipe
DLice DLice	$DL_{ice,p2} = 49.43 \text{ lbf}$	Total Weight of Ice
$\frac{\text{DL}_{\text{ice}}}{\text{H}_{\text{pipe}}}$	$DL_{ice.p2_linear} = 9.89 \cdot plf$	Linear Ice Load on Pipe
Fp2i = Fpi	$F_{p2i} = 9.71 lbf$	Wind Load with Ice
Fp2inlinear := Fpi_linear	$F_{p2i_linear} = 2 \cdot plf$	Linear Wind Load with Ice on Pipe
$F_{Ehp2} := Weight_{total} \cdot A_s \cdot C_s$	$F_{Ehp2} = 5.06 \text{ lbf}$	Total Lateral Earthquake Load
$F_{Ehp2_linear} := \frac{F_{Ehp2}}{H_{pipe}}$	$F_{Ehp2_linear} = 1.01 \cdot plf$	Linear Lateral Earthquake Load
FEXD2 := 0.2 · SDS · Weighttotal	$F_{Evp2} = 0.67 lbf$	Total Vertical Earthquake Load
$F_{\text{Exp2,linear}} := \frac{F_{\text{Evp2}}}{H_{\text{pipe}}}$	$F_{Evp2_linear} = 0.13 \cdot plf$	Linear Vertical Earthquake Load

PL3/8x3:		
HeightWidth/Diameterheight := 120inwidth := 3in	Depth/DiameterWeightdepth := 0.375inweight := 3.83plf	<u>Shape</u> ● Flat ○ Round
FEMILlinear = FF_linear	$F_{FM1_linear} = 14 \cdot plf$	Linear Wind Load on Front Face
FSM1_linear := Fs_linear	$F_{SM1_linear} = 2 \cdot plf$	Linear Wind Load on Side Face
DLice Millinear. := DLice height	$DL_{ice.M1_linear} = 7 \cdot plf$	Linear Ice Load on Member
FEIMILINGER = FFI_linear	$F_{FiM1_linear} = 4 \cdot plf$	Linear Wind Load with Ice on Front Face
Fsimilinear := Fsi_linear	$F_{SiM1_linear} = 2 \cdot plf$	Linear Wind Load with Ice on Side Face
FEMIN:= FF	$F_{FM1} = 138.74 \cdot lbf$	Wind Load on Front Face
FSML:= FS	$F_{SM1} = 17.34 \cdot lbf$	Wind Load on Side Face
FEIMIN:= F _{Fi}	$F_{FiM1} = 37.53 \cdot lbf$	Wind Load with Ice on Front Face
F _{SIMM} := F _{Si}	$F_{SiM1} = 23.58 \cdot lbf$	Wind Load with Ice on Side Face
DLice DLice	$DL_{ice.M1} = 69.97 lbf$	Total Weight of Ice
Wtww.:= Weighttotal	$Wt_{M1} = 38.3 \text{ lbf}$	Total Weight of member
$F_{EhML}:= Weight_{total} A_s C_s$	$F_{EhM1} = 5.11 lbf$	Total Lateral Earthquake Load
$F_{EhM1} = \frac{F_{EhM1}}{height}$	$F_{EhM1_linear} = 0.51 \cdot plf$	Linear Lateral Earthquake Load
FEXML := 0.2.S _{DS} .Weight _{total}	$F_{EvM1} = 0.68 \text{ lbf}$	Total Vertical Earthquake Load
$F_{ExM1_linear} := \frac{F_{EvM1}}{height}$	$F_{EvM1_linear} = 0.07 \cdot plf$	Linear Vertical Earthquake Load

















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Company Designer Job Number Model Name

1

1 1

MWMKE00116

Equipment Platform

: Fullerton Engineering Consultants, LLC AA

June 2, 2022 1:57 PM Checked By: BK

(Global) Model Settings

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation?	Yes
Increase Nailing Capacity for Wind?	Yes
Include Warping?	Yes
Trans Load Btwn Intersecting Wood Wall?	Yes
Area Load Mesh (in^2)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Include P-Delta for Walls?	Yes
Automatically Iterate Stiffness for Walls?	Yes
Max Iterations for Wall Stiffness	3
Gravity Acceleration (in/sec^2)	386.4
Wall Mesh Size (in)	12
Eigensolution Convergence Tol. (1.E-)	4
Vertical Axis	Y
Global Member Orientation Plane	XZ
Static Solver	Sparse Accelerated
Dynamic Solver	Accelerated Solver
Hot Rolled Steel Code	AISC 15th(360-16): LRFD
Adjust Stiffness?	Yes(Iterative)
RISAConnection Code	AISC 15th(360-16): LRFD
Cold Formed Steel Code	AISI S100-16: LRFD
Wood Code	None
Wood Temperature	< 100F
Concrete Code	None
Masonry Code	None
Aluminum Code	None - Building
Stainless Steel Code	None



(Global) Model Settings, Continued

Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	Exact Integration
Parme Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections?	Yes
Use Cracked Sections Slab?	No
Bad Framing Warnings?	No
Unused Force Warnings?	Yes
Min 1 Bar Diam. Spacing?	No
Concrete Rebar Set	REBAR_SET_ASTMA615
Min % Steel for Column	1
Max % Steel for Column	8

Seismic Code	ASCE 7-16
Seismic Base Elevation (in)	Not Entered
Add Base Weight?	Yes
Ct X	.02
Ct Z	.02
T X (sec)	Not Entered
T Z (sec)	Not Entered
RX	3
RZ	3
Ct Exp. X	.75
Ct Exp. Z	.75
SD1	1
SDS	1
S1	1
TL (sec)	5
Risk Cat	l or ll
Drift Cat	Other
Om Z	1
Om X	1
Cd Z	1
Cd X	1
Rho Z	1
Rho X	1

Hot Rolled Steel Design Parameters

	Label	Shape	Length[in]	Lbyy[in]	Lbzz[in]	Lcomp top[in]	Lcomp bot[in]	L-torg	Kyy	Kzz	Cb	Function
1	M1	C8X11.5	120	Ő	0	0	0	0	.65	.65		Lateral
2	M2	C8X11.5	120	0	0	0	0	0	.65	.65		Lateral
3	M3	C8X11.5	96	0	0	0	0	0	1	1		Lateral
4	M4	C8X11.5	96	0	0	0	0	0	1	1		Lateral
5	M5	C8X11.5	96	0	0	0	0	0	1	1		Lateral
6	M6	C8X11.5	96	0	0	0	0	0	1	1		Lateral
7	M7	L2x2x4	42			Lbyy			.65	.65		Lateral
8	M8	L2x2x4	42			Lbyy			.65	.65		Lateral
9	M9	L2x2x4	42			Lbyy			.65	.65		Lateral
10	M10	L2x2x4	42			Lbyy			.65	.65		Lateral
11	M11	L2x2x4	42			Lbyy			.65	.65		Lateral
12	M12	L2x2x4	42			Lbyy			.65	.65		Lateral
13	M13	L2x2x4	42			Lbyy			.65	.65		Lateral
14	M14	L2x2x4	42			Lbyy			.65	.65		Lateral
15	M15	L2x2x4	42			Lbyy			.65	.65		Lateral
16	M16	L2x2x4	42			Lbyy			.65	.65		Lateral



Hot Rolled Steel Design Parameters (Continued)

	Label	Shape	Length[in]	Lbyy[in]	Lbzz[in]	Lcomp top[in]	Lcomp bot[in]	L-torq	Kyy	Kzz	Cb	Function
17	M17	L2x2x4	42			Lbyy		-	.65	.65		Lateral
18	M18	L2x2x4	42			Lbyy			.65	.65		Lateral
19	M19	L2x2x4	42			Lbyy			.65	.65		Lateral
20	M20	L2x2x4	42			Lbyy			.65	.65		Lateral
21	M21	L2x2x4	42			Lbyy			.65	.65		Lateral
22	M22	L2x2x4	42			Lbyy			.65	.65		Lateral
23	M23	L2x2x4	96			Lbyy			1	1		Lateral
24	M24	L2x2x4	120			Lbyy			1	1		Lateral
25	M25	L2x2x4	96			Lbyy			1	1		Lateral
26	M26	L2x2x4	78.667			Lbvy			1	1		Lateral
27	M27	L2x2x4	4			Lbyy			1	1		Lateral
28	M28	L2x2x4	4			Lbyy			1	1		Lateral
29	M29	L2x2x4	96			Lbyy			1	1		Lateral
30	M30	L2x2x4	120			Lbvy			1	1		Lateral
31	M31	L2x2x4	96			Lbyy			1	1		Lateral
32	M32	L2x2x4	78.667			Lbyy			1	1		Lateral
33	M34	L4X4X4	111.485			Lbyy						Lateral
34	M40	PIPE 3.0	60	60	60	60	60	60	2.1	2.1		Lateral
35	M41	PIPE 3.0	60	60	60	60	60	60	2.1	2.1		Lateral
36	M42	PL3/8"x3"	4			Lbyy			1	1		Lateral
37	M43	PL3/8"x3"	96			Lbyy			1	1		Lateral
38	M44	PL3/8"x3"	120			Lbyy			1	1		Lateral
39	M45	PL3/8"x3"	96			Lbyy			1	1		Lateral
40	M46	PL3/8"x3"	78.667			Lbyy			1	1		Lateral
41	M103	W10X15	96	0	0	0	0	0	.8	.8		Lateral
42	M104	W10X15	96	0	0	0	0	0	.8	.8		Lateral
43	M105	W12X22	240	84	84	84	84	84	1	1		Lateral
44	M117	W12X22	240	84	84	84	84	84	1	1		Lateral
45	M116A	L4x4x4	111.485			Lbyy						Lateral

Material Takeoff

	Material	Size	Pieces	Length[in]	Weight[LB]
1	General			••••	• • •
2	RIGID		66	1107.4	0
3	Total General		66	1107.4	0
4					
5	Hot Rolled Steel				
6	A36 Gr.36	C8X11.5	6	624	596.303
7	A36 Gr.36	L2x2x4	26	1461.3	391.177
8	A36 Gr.36	L4X4X4	1	111.5	61.014
9	A36 Gr.36	L4x4x4	1	111.5	61.014
10	A36 Gr.36	PL3/8"x3"	5	394.7	125.903
11	A53 Gr. B	PIPE 3.0	2	120	70.438
12	A992	W10X15	2	192	240.1
13	A992	W12X22	2	480	882
14	Total HR Steel		45	3495	2427.948
15					
16	Cold Formed Steel				
17	A570 Gr.33	P1000	5	290	36.759
18	Total CF Steel		5	290	36.759



Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distribut	Area(Me	.Surface(
1	DL	None		-1		5			1	,
2	WL(0)	None				5		69		
3	WL(90)	None				5		64		
4	EH(0)	None				5		98	1	
5	EH(90)	None				5		98	1	
6	EV	None				5		94	1	
7	LL	None							8	
8	SL	None							1	
9	BLC 1 Transient Area Loads	None						35		
10	BLC 8 Transient Area Loads	None						35		
11	BLC 4 Transient Area Loads	None						35		
12	BLC 6 Transient Area Loads	None						35		
13	BLC 5 Transient Area Loads	None						35		
14	BLC 7 Transient Area Loads	None						64		

Load Combinations

	Description	So	P	S	BLC	Fac	BLC	Fac	BLC	Fac	.BLC	Fac												
1	1.4*DL	Yes	Υ		1	1.4																		
2	1.2*DL + 1.0* WL(0	Yes	Υ		1	1.2	2	1	8	.5														
3	1.2*DL + 1.0*WL(9	Yes	Υ		1	1.2	3	1	8	.5														
4	1.2*DL + 1.0 * WL(Yes	Y		1	1.2	2	-1	8	.5														
5	1.2*DL + 1.0*WL(2	Yes	Υ		1	1.2	3	-1	8	.5														
6	1.2*DL+1.0*EH(0)+	Yes	Y		1	1.2	4	1	6	1														
7	1.2*DL+1.0*EH(0)+	Yes	Υ		1	1.2	4	1	6	-1														
8	1.2*DL+1.0*EH(90)	Yes	Υ		1	1.2	5	1	6	1														
9	1.2*DL+1.0*EH(90)	Yes	Υ		1	1.2	5	1	6	-1														
10	1.2*DL+1.0*EH(18	Yes	Υ		1	1.2	4	-1	6	1														
11	1.2*DL+1.0*EH(18	Yes	Υ		1	1.2	4	-1	6	-1														
12	1.2*DL+1.0*EH(27	Yes	Υ		1	1.2	5	-1	6	1														
13	1.2*DL+1.0*EH(27	Yes	Υ		1	1.2	5	-1	6	-1														
14	0.9*DL+1.0*WL(0)	Yes	Υ		1	.9	2	1																
15	0.9*DL+1.0*WL(90)	Yes	Υ		1	.9	3	1																
16	0.9*DL+1.0*WL(180)	Yes	Υ		1	.9	2	-1																
17	0.9*DL+1.0*WL(270)	Yes	Υ		1	.9	3	-1																
18	0.9*DL+1.0*EH(0)	Yes	Υ		1	.9	4	1	6	-1														
19	0.9*DL+1.0*EH(0)	Yes	Υ		1	.9	4	1	6	1														
20	0.9*DL+1.0*EH(90)	Yes	Υ		1	.9	5	1	6	-1														
21	0.9*DL+1.0*EH(90)	Yes	Υ		1	.9	5	1	6	1														
22	0.9*DL+1.0*EH(18	Yes	Υ		1	.9	4	-1	6	-1														
23	0.9*DL+1.0*EH(18	Yes	Υ		1	.9	4	-1	6	1														
24	0.9*DL+1.0*EH(27	Yes	Υ		1	.9	5	-1	6	-1														
25	0.9*DL+1.0*EH(27	Yes	Υ		1	.9	5	-1	6	1														
26	1.2*DL+1.6*LL+0.5	Yes	Υ		1	1.2	7	1.6	8	.5														
27	1.2*DL+1.6*LL+0.5	Yes	Υ		1	1.2	7	1.6	2	.5														
28	1.2*DL+1.6*LL+0.5	Yes	Υ		1	1.2	7	1.6	3	.5														
29	1.2*DL+1.6*LL+0.5	Yes	Υ		1	1.2	7	1.6	2	5														
30	1.2*DL+1.6*LL+0.5	Yes	Y		1	1.2	7	1.6	3	5														
31	DL	Yes	Υ		1	1																		



Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [lb-in]	LC	MY [lb-in]	LC	MZ [lb-in]	LC
1	N13	max	2770.443	16	2125.02	26	1709.421	2	.545	14	Ō	31	<u> </u>	31
2		min	-6767.404	2	504.318	16	-1713.294	4	-5.418	29	0	1	0	1
3	N14	max	4666.039	28	4431.327	26	811.996	14	.014	14	0	31	0	31
4		min	503.969	17	764.569	16	-839.217	4	139	29	0	1	0	1
5	N235A	max	3129.864	14	2129.09	26	1698.538	2	5.403	27	0	31	0	31
6		min	-6189.022	4	390.421	14	-1698.425	4	.297	16	0	1	0	1
7	N236A	max	4398.243	28	4521.289	26	464.724	2	.139	27	0	31	0	31
8		min	248.395	17	505.132	14	-434.599	16	.008	16	0	1	0	1
9	N153	max	LOCKED		LOCKED		LOCKED		NC		NC		NC	
10		min	LOCKED		LOCKED		LOCKED		NC		NC		NC	
11	N151	max	LOCKED		LOCKED		LOCKED		NC		NC		NC	
12		min	LOCKED		LOCKED		LOCKED		NC		NC		NC	
13	N152	max	LOCKED		LOCKED		LOCKED		NC		NC		NC	
14		min	LOCKED		LOCKED		LOCKED		NC		NC		NC	
15	N150	max	NC		LOCKED		LOCKED		NC		NC		NC	
16		min	NC		LOCKED		LOCKED		NC		NC		NC	
17	Totals:	max	3618.706	3	13206.726	26	4676.997	2						
18		min	-3618.702	17	3118.264	22	-4676.985	16						

Max. Stress Ratio<1

Members are adequate

Envelope AISC 15th(360-16): LRFD Steel Code Checks

	Member	Shape	Coc	de Che	ok	Loc[in]	LC	Sł	<u>near Ch</u>	Loc[in]	Dir	LC ph	hi*Pncp	<u>phi*Pnt [.</u>	<u>phi*Mn</u>	phi*Mn	Cb	Eqn
1	M1	C8X11.5		.365	\sim	85	4		.212	10	y	26 1	<u>09188</u>	<u>109188</u>	40231.28	312012	1.589	H1-1b
2	M11	L2x2x4		.341		0	5		.012	0	z	5 23	3536.63	30585.6	8291.204	18922.19	2.578	H2-1
3	M21	L2x2x4		.297		0	2		.011	0	V	2 23	3536.63	30585.6	8291.204	18922.19	1.789	H2-1
4	M6	C8X11.5		.290		4	30		.104	0	z	26 1	09188	<u>109188</u>	40231.28	312012	1.437	H1-1b
5	M5	C8X11.5		.285		92	26		.096	92	z	26 1	09188	109188	40231.28	312012	1.433	H1-1b
6	M105	W12X22		.280		132.5	27		.065	122.5	v	26 14	42305	291600	164700	981699	1	H1-1b
7	M117	W12X22		.279		132.5	29		.066	122.5	ý	26 14	42305	291600	164700	981699	1	H1-1b
8	M2	C8X11.5		.264		120	2		.347	40	y	2 1	09188	<u>109188</u>	40231.28	312012	1.528	H1-1b
9	M40	PIPE 3.0		.251		0	4		.165	0		4 36	6138.4	65205	68985	68985	1	H1-1b
10	M41	PIPE 3.0		.242		0	4		.167	0		4 36	6138.4	65205	68985	68985	1	H1-1b
11	M116A	L4x4x4		.242		54.5	16		.004	0	y	2 21	1507.2	62532	37651.1	60842.4	1.136	H2-1
12	M34	L4X4X4		.242		56.9	14		.004	111	V	4 21	1507.2	62532	37651.1	60842.4	1.136	H2-1
13	M7	L2x2x4		.216		0	30		.065	0	ý	2 23	3536.63	30585.6	8291.204	18922.19	2.389	H2-1
14	M14	L2x2x4		.192		0	28		.059	0	z	2 23	3536.63	30585.6	8291.204	18922.19	2.38	H2-1
15	M24	L2x2x4		.188		60	2		.012	5	z	2 22	218.05	30585.6	8291.204	13882.5	1.151	H2-1
16	M10	L2x2x4		.156		0	5		.069	0	V	2 23	3536.63	30585.6	8291.204	18922.19	2.272	H2-1
17	M30	L2x2x4		.151		41.25	2		.027	120	ý	30 22	218.05	30585.6	8291.204	14540.7	1.312	H2-1
18	M20	L2x2x4		.147		0	4		.014	0	V	16 23	3536.63	30585.6	8291.204	18922.19	2.359	H2-1
19	M19	L2x2x4		.142		0	3		.016	0	ý	4 23	3536.63	30585.6	8291.204	18922.19	2.708	H2-1
20	M31	L2x2x4		.137		4	30		.032	4	y	5 34	465.703	30585.6	8291.204	17715.1	2.325	H2-1
21	M22	L2x2x4		.136		0	2		.038	0	ý	4 23	3536.63	30585.6	8291.204	18922.19	1.646	H2-1
22	M12	L2x2x4		.135		0	5		.033	0	y	3 23	3536.63	30585.6	8291.204	18399.3	1.27	H2-1
23	M25	L2x2x4		.125		48	3		.018	4	ý	5 34	465.703	30585.6	8291.204	14928.9	1.139	H2-1
24	M18	L2x2x4		.114		0	5		.012	0	v	5 23	3536.63	30585.6	8291.204	18922.19	2.32	H2-1
25	M8	L2x2x4		.111		0	4		.037	0	ý	5 23	3536.63	30585.6	8291.204	18922.19	2.274	H2-1
26	M3	C8X11.5		.108		84	3		.153	96	z	3 1	09188	109188	40231.28	312012	1.486	H1-1b
27	M15	L2x2x4		.107		0	4		.012	0	v	3 23	3536.63	30585.6	8291.204	18922.19	2.579	H2-1
28	M9	L2x2x4		.104		0	4		.037	0	V	5 23	3536.6	30585.6	8291.204	18922.19	2.196	H2-1
29	M4	C8X11.5		.103		84	5		.104	62	z	5 1	09188	109188	40231.28	312012	1.446	H1-1b
30	M23	L2x2x4		.101		53	5		.014	4	z	5 34	465.703	30585.6	8291.204	15190.3	1.206	H2-1
31	M29	L2x2x4		.101		50	5		.020	92	y	27 34	465.703	30585.6	8291.204	14888.0	1.129	H2-1
32	M17	L2x2x4		.096		0	2		.012	0	V	5 23	3536.63	30585.6	8291.204	18922.19	2.371	H2-1
33	M13	L2x2x4		.090		0	2		.041	0	V	5 23	3536.63	30585.6	8291.204	18922.19	2.252	H2-1
34	M16	L2x2x4		.090		0	4		.013	0	y	5 23	3536.63	30585.6	8291.204	18922.19	2.481	H2-1



Envelope AISC 15th(360-16): LRFD Steel Code Checks (Continued)

	Member	Shape	Code Ch	eck	Loc[in]	LC	S	<u>hear Ch</u>	Loc[in]	Dir	LC	phi*Pnc	.phi*Pnt [.	phi*Mn	phi*Mn	Cb	Eqn
35	M104	W10X15	.089		51	4		.064	51	z	2	 189395	198450	103500	720000	1.198	H1-1b
36	M32	L2x2x4	.079		40.9	2		.016	0	V	5	5161.219	30585.6	8291.204	16738.2	1.44	H2-1
37	M103	W10X15	.071		48	5		.006	96	y	26	189395	198450	103500	720000	1.109	H1-1b
38	M26	L2x2x4	.060		31.9	4		.015	78.6	z	2	5161.219	30585.6	8291.204	16050.85	1.208	H2-1
39	M28	L2x2x4	.003		1.292	5		.000	4	z	16	30414.0	30585.6	8291.204	18922.19	1.136	H2-1
40	M27	L2x2x4	.000		2	4		.000	4	z	16	30414.0	30585.6	8291.204	18922.19	1.136	H2-1
41	M42	PL3/8"x3"	.000		0	15		.000	0	z	16	33922.0	36450	3417.196	27337.5	1.136	H1-1b*
42	M43	PL3/8"x3"	.000		0	31		.000	0	V	31	323.18	36450	3417.196	13620.3	1	H1-1a
43	M44	PL3/8"x3"	.000		0	31		.000	0	ý	31	206.835	36450	3417.196	10896.24	1	H1-1a
44	M45	PL3/8"x3"	.000		0	31		.000	0	V	31	323.18	36450	3417.196	13620.3	1	H1-1a
45	M46	PL3/8"x3"	.000		0	31		.000	0	ý	31	481.289	36450	3417.196	16621.3	1	H1-1a

Equipment Platform Connection Calculations

New equipment platform will be attached to existing parapet wall and elevated roof wall via (4) Thru-Bolts 5/8"Ø

Maximum Reactions from Risa Mount Analysis per one thru-bolt:

Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [lb-in]	LC	MY [lb-in]	LC	MZ [lb-in]	LC	
1	N13	max	2770.443	16	2125.02	26	1709.421	2	.545	14	0	31	0	31	
2		min	-6767.404	2	504.318	16	-1713.294	4	-5.418	29	0	1	0	1	
3	N14	max	4666.039	28	4431.327	26	811.996	14	.014	14	0	31	0	31	
4		min	503.969	17	764.569	16	-839.217	4	139	29	0	1	0	1	
5	N235A	max	3129.864	14	2129.09	26	1698.538	2	5.403	27	0	31	0	31	
6		min	-6189.022	4	390.421	14	-1698.425	4	.297	16	0	1	0	1	
7	N236A	max	4398.243	28	4521.289	26	464.724	2	.139	27	0	31	0	31	
8		min	248.395	17	505.132	14	-434.599	16	.008	16	0	1	0	1	
X:= ⁶⁷	$\frac{67.404}{4}$ lbf = 169	91.85 lb1	ſ			Maximum Factored Reaction - X direction									
Y.:= ²¹	$\frac{25.02}{4}$ lbf = 531.2	25 lbf				Maximum Factored Reaction - Y direction									
<u>Z</u> := <u>17</u>	$\frac{13.294}{4}$ lbf = 428	.32 lbf				Maximum Factored Reaction - Z direction									
Pt := X						P _t =	1691.85 lbf			Fa	Factored Tensile Force				
₽,:= √	$Y^2 + Z^2$		P _V =	= 682.42 lbf			Fa	Factored Shear Force							
db.:= 0.	625in						Dia	Diameter of thru-bolt							
Ab := 0.	$25\pi \cdot d_b^2$	A _b =	= 0.31·in ²			Are	Area of thru-bolt								
Pt.bolt.	= P _t	P _{t_bo}	_{olt} = 1691.85	lbf		Te	Tension at each thru-bolt								
Purbolt.:	= P _v					P _{v_b}	_{olt} = 682.42 l	bf		Sh	Shear at each thru-bolt				



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NET WT.

UNIT WT.

LENGTH 15 3/4 in 14 1/2 in

PARTS LIST

PART DESCRIPTION

3.28 8.13

10 in

SLIDER BRACKET ANGLE SLIDER BRACKET BENT PLATE SLIDER BRACKET WALL ANGLE 5/8" x 2" HDG HEX BOLT GR5 5/8" HDG USS FLATWASHER

X-SLD-BP

PART NO X-SLD-A X-SLD3

QTY

ITEM

4 2

~ 2 ო 4 2

G5802 G58FW G58LW

∞ ∞ ∞ ∞

13.12 16.26 12.20 2.16 0.56 0.56 0.21 1.04 0.27 0.27

6.10 0.27 0.07 0.03

1/8 in

0.13 0.03

5/8" HDG HEAVY 2H HEX NUT

5/8" HDG LOCKWASHER

3/32 in 1/8 in

0.57 2.65 2.95 51.93

0.07 0.66 0.74 TOTAL WT. #

1/2" X 2-1/2" X 4-1/2" X 2" GALV. U-BOLT 1/2" X 3" X 5" X 2" GALV U-BOLT

X-UB1212 X-UB1300

7

1/2" HDG HEAVY 2H HEX NUT 1/2" HDG USS FLATWASHER

1/2" HDG LOCKWASHER

G12LW

6 œ 10 7

G58NUT G12FW G12NUT

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9 2 œ 8 4 4





























